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(54) **MATCHING AND PATTERN CONTROL FOR DUAL BAND CONCENTRIC ANTENNA FEED**

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(73) Assignee: **Honeywell International Inc.**, Morris Plains, NJ (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 150 days.

(21) Appl. No.: **14/163,351**

(22) Filed: **Jan. 24, 2014**

(65) **Prior Publication Data**

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(51) **Int. Cl.**

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H01Q 5/335	(2015.01)
H01Q 13/08	(2006.01)
H01Q 19/06	(2006.01)
H01P 1/161	(2006.01)
H01Q 13/02	(2006.01)

(52) **U.S. Cl.**

CPC ***H01Q 5/321*** (2015.01); ***H01P 1/161*** (2013.01); ***H01Q 5/335*** (2015.01); ***H01Q 13/0258*** (2013.01); ***H01Q 13/08*** (2013.01); ***H01Q 19/062*** (2013.01)

(58) **Field of Classification Search**

CPC H01Q 5/321; H01Q 13/08; H01Q 19/062; H01Q 5/335

USPC 343/795, 753

See application file for complete search history.

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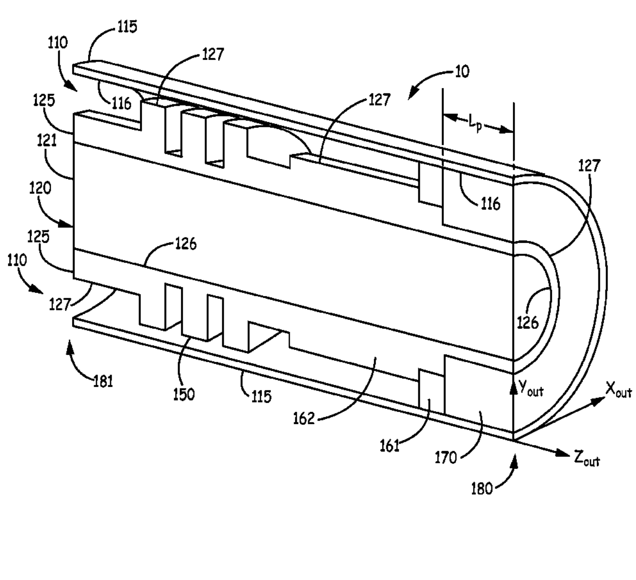
Primary Examiner — Jean B Jeanglaude

(74) *Attorney, Agent, or Firm* — Fogg & Powers LLC

(57) **ABSTRACT**

A dual band concentric antenna feed is provided. The dual band concentric antenna feed includes an outer conductive tube and an inner conductive tube. The inner conductive tube is positioned inside the outer conductive tube and is coaxially aligned to a shared axis. A coaxial waveguide formed between the inner surface of the outer conductive tube and the outer surface of the inner conductive tube supports a first frequency band. A circular waveguide formed within of the inner conductive tube supports a second frequency band. The dual band concentric antenna feed also includes at least one transformer, a filter, and a plug in the coaxial waveguide. An impedance locus associated with the filter is high-frequency capacitive within the first frequency band and low-frequency inductive within the first frequency band. The plug is positioned near an aperture end of the concentric antenna feed.

20 Claims, 15 Drawing Sheets



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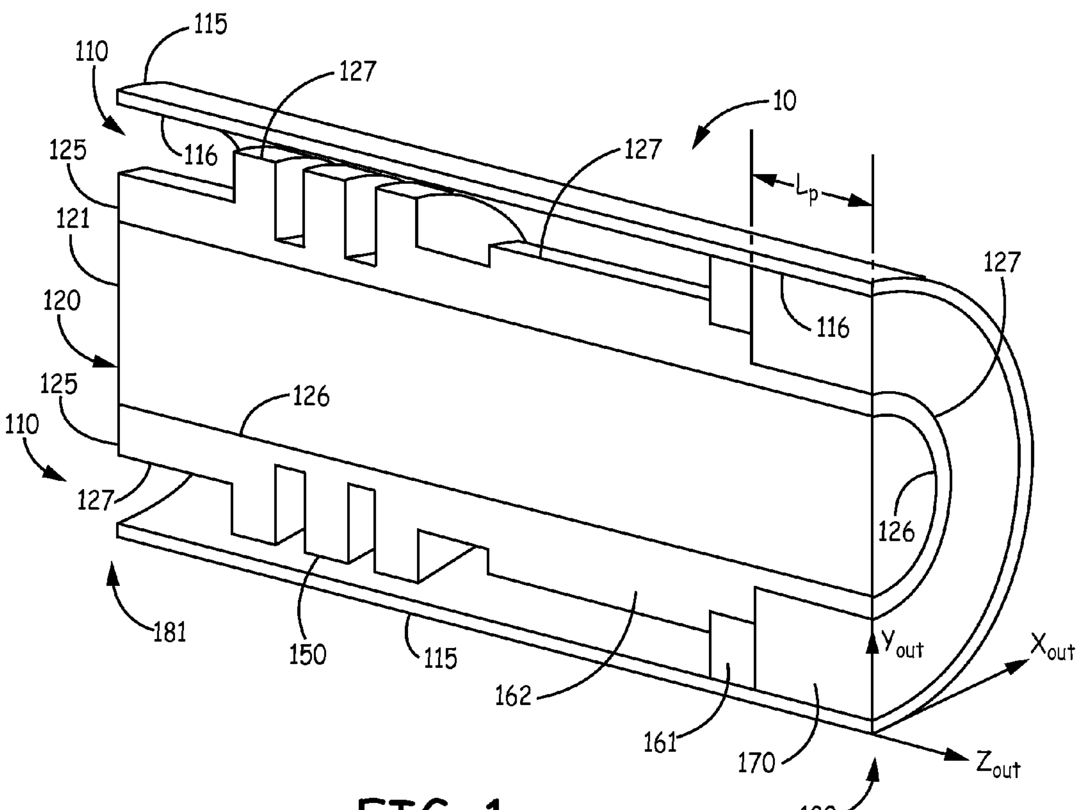
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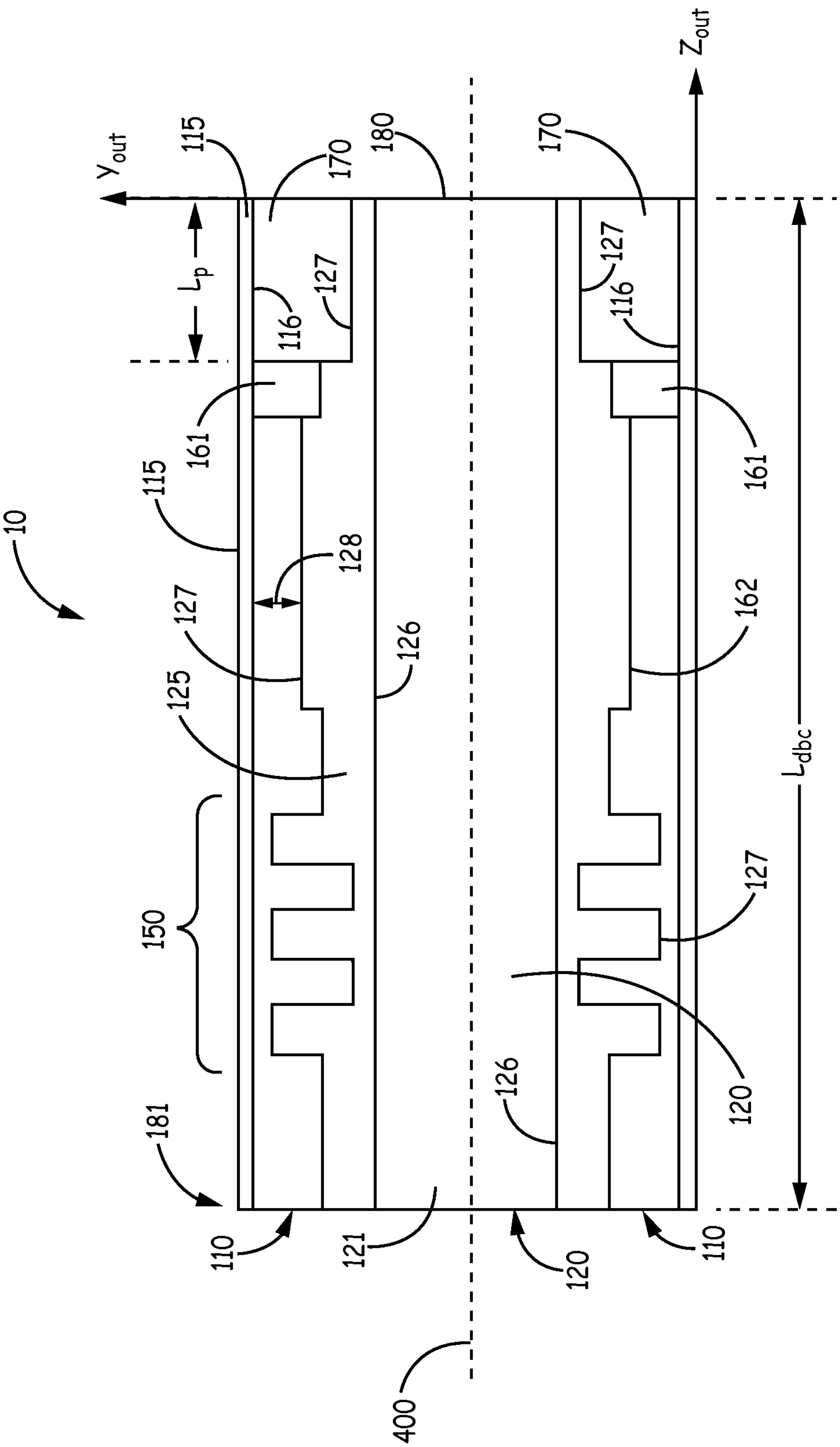
Y_{out}
X_{out}
181
150
115
162
161
170
Z_{out}
180

FIG. 1



10
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180
170
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116
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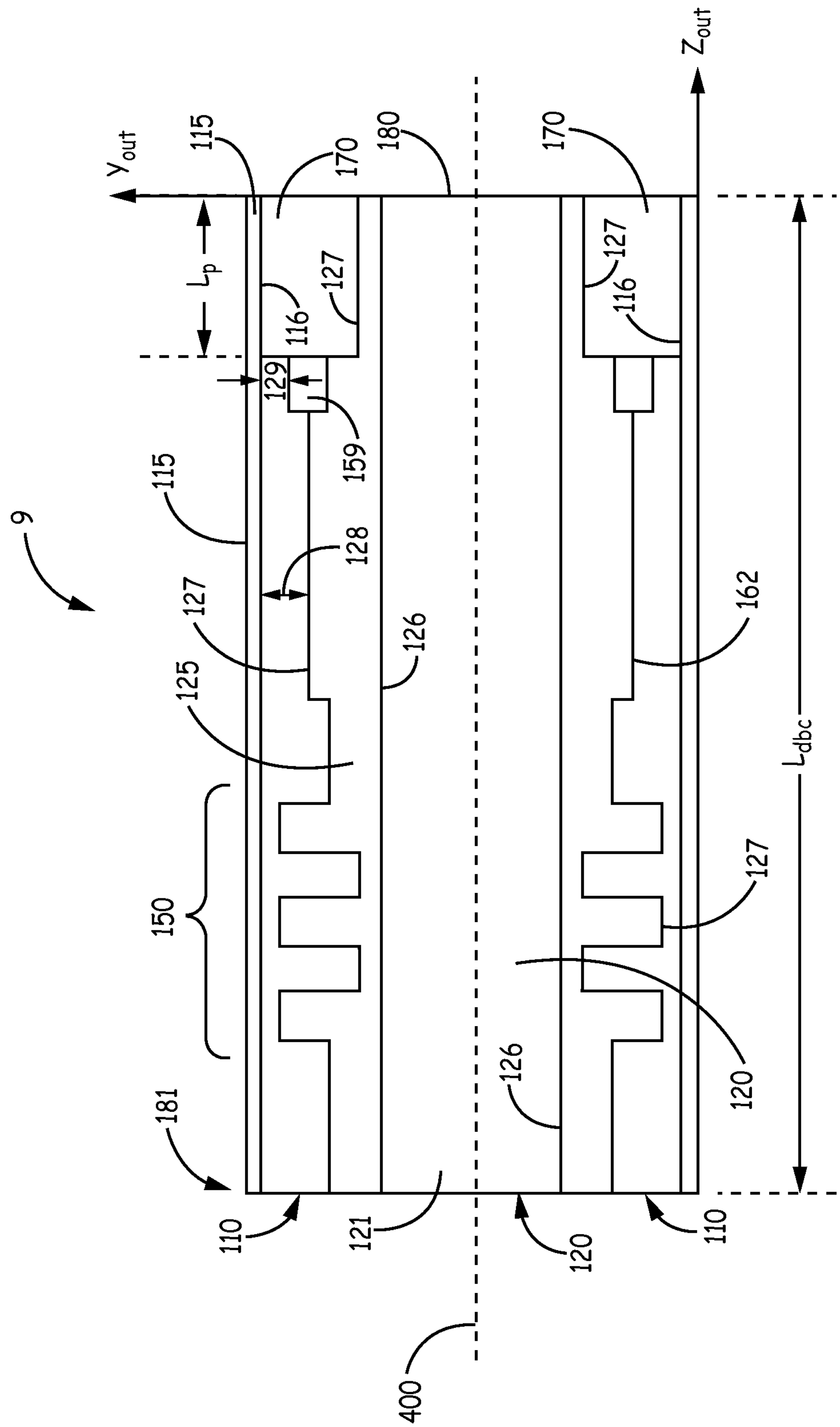
121
120
400
162
Ldbc

FIG. 2A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125
126
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181
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120
110
400
Y_{out}
Z_{out}
L_p
L_{dbc}

FIG. 2B

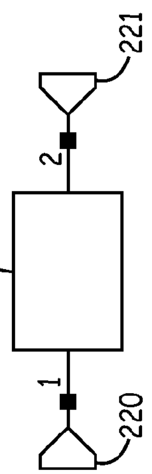


FIG. 3A

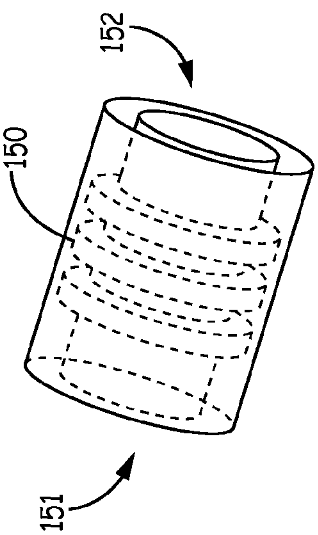


FIG. 3B

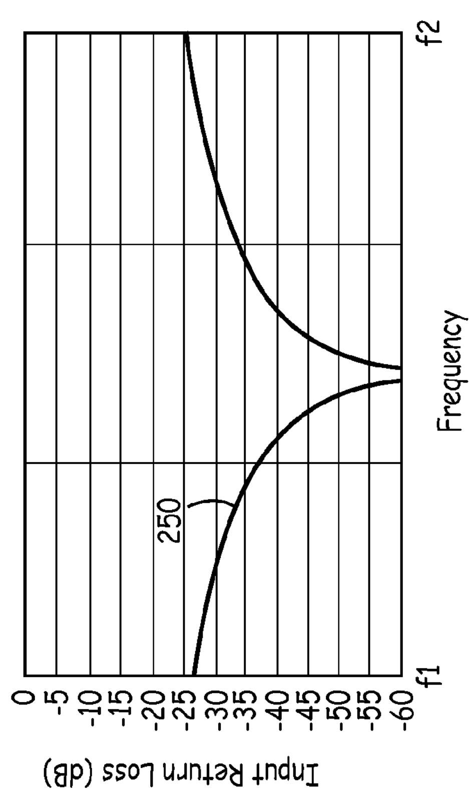


FIG. 3C

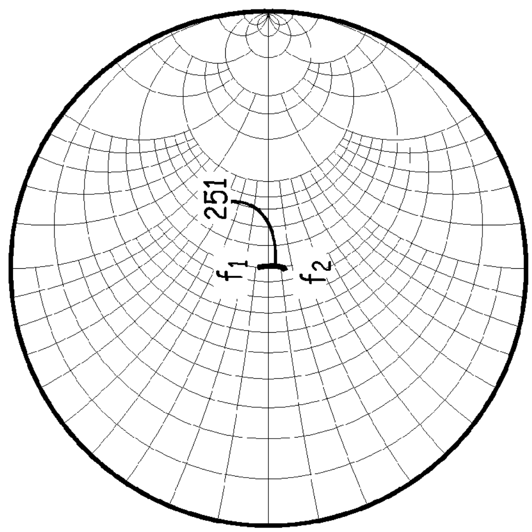
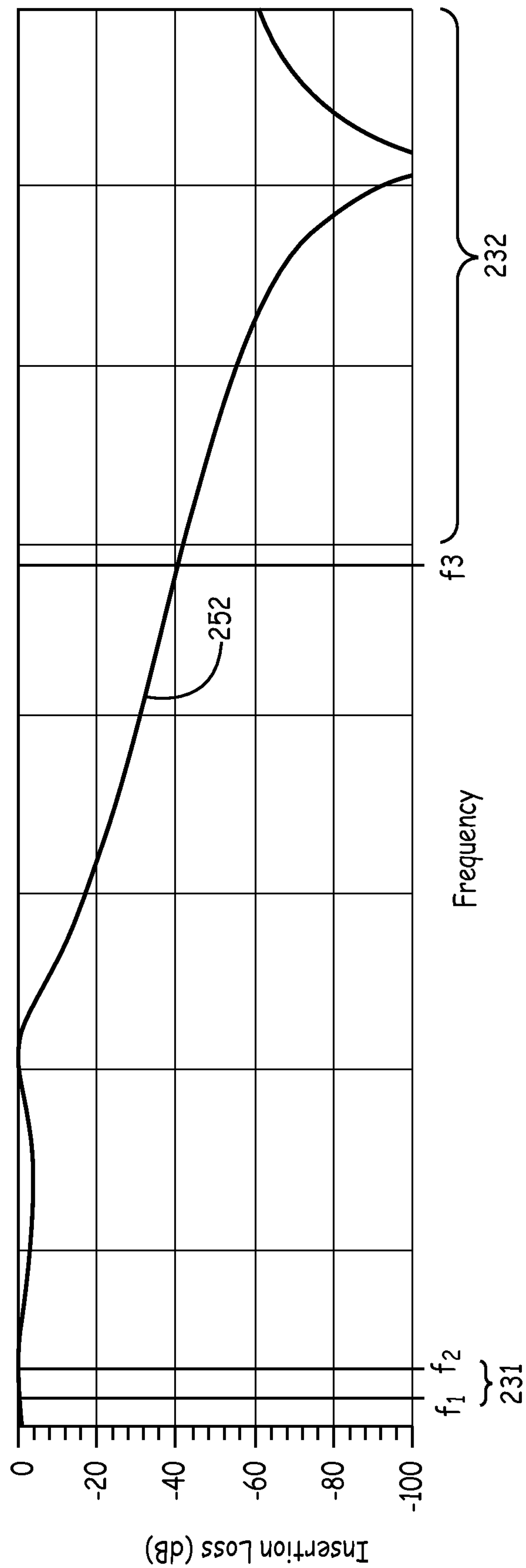


FIG. 3D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-20
-40
-60
-80
-100
Frequency
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f2
231
f3
232
252

FIG. 4

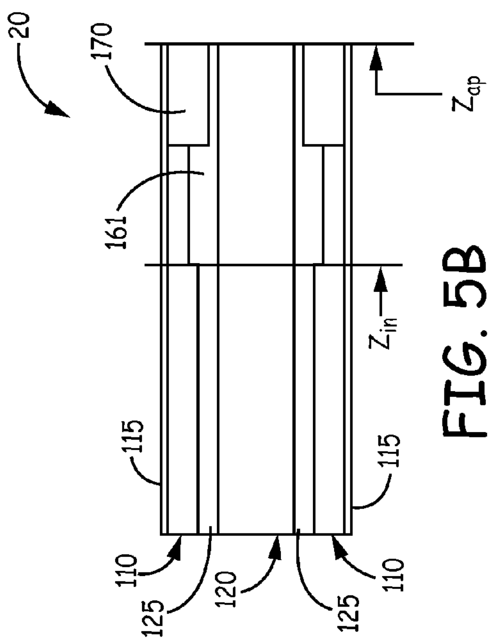


FIG. 5B

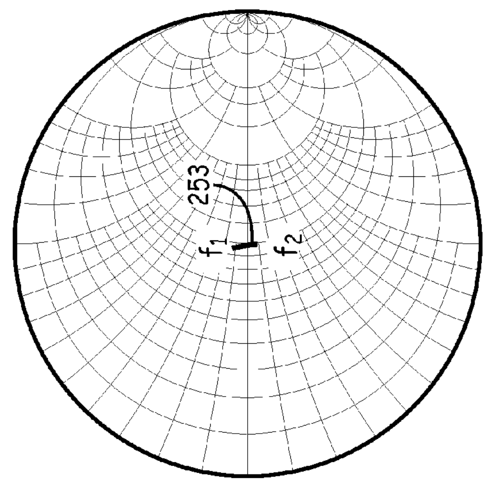


FIG. 5D

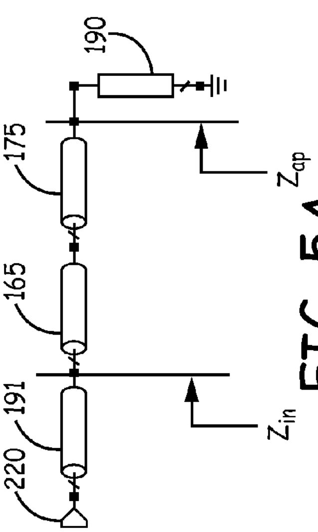


FIG. 5A

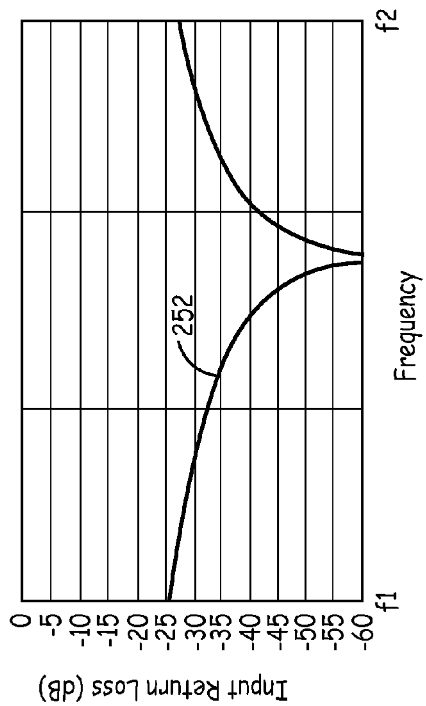


FIG. 5C

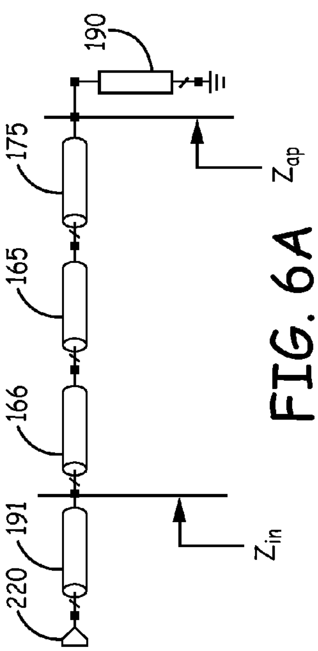


FIG. 6A

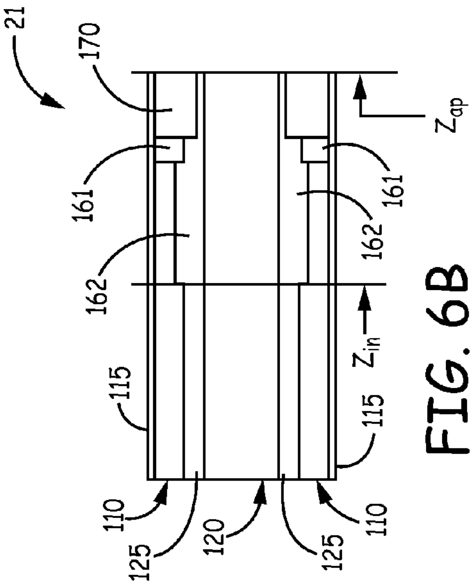


FIG. 6B

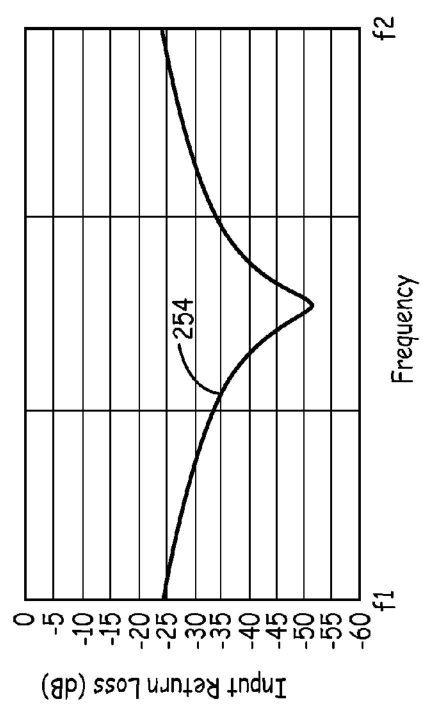


FIG. 6C

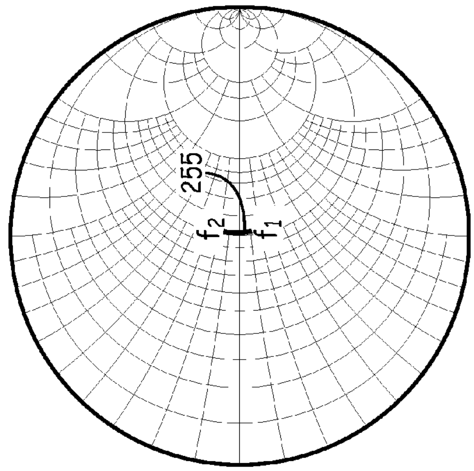


FIG. 6D

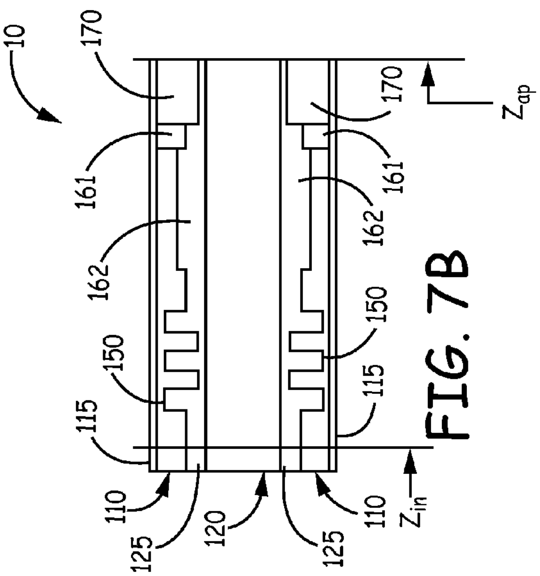


FIG. 7B

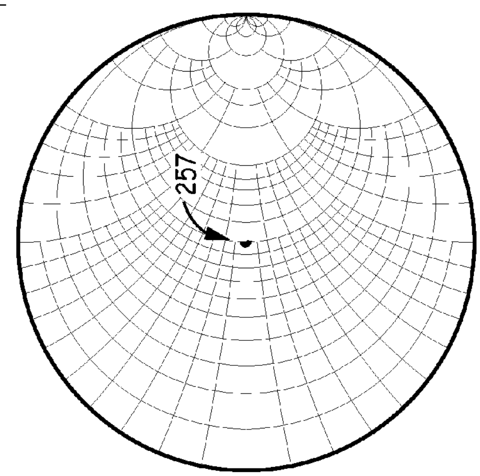


FIG. 7D

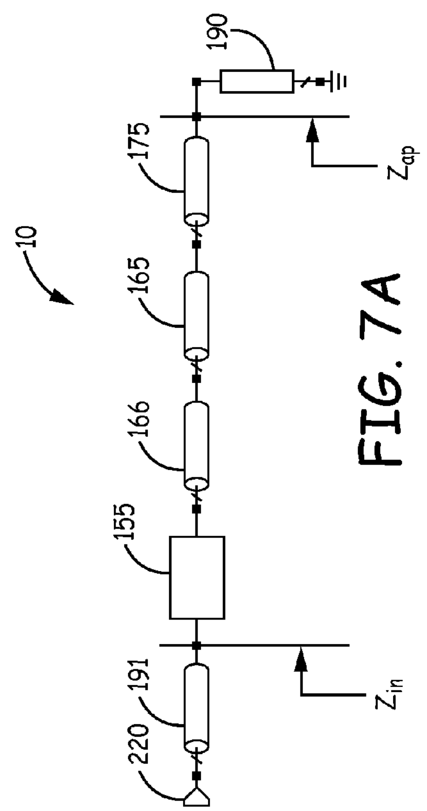


FIG. 7A

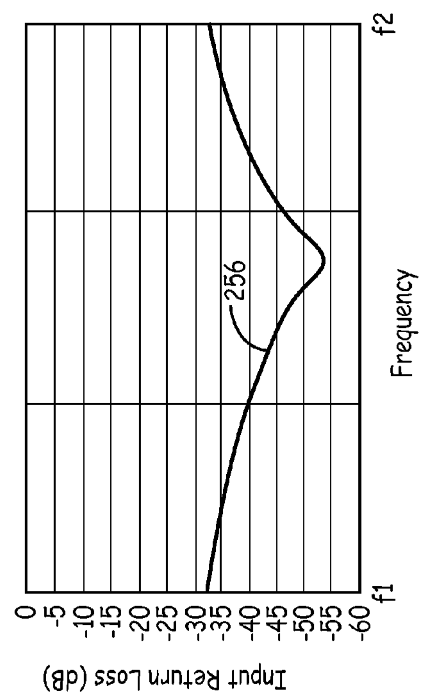


FIG. 7C

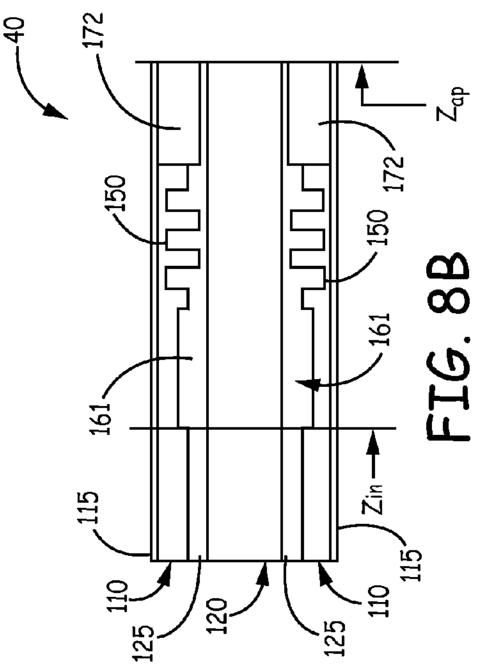


FIG. 8B

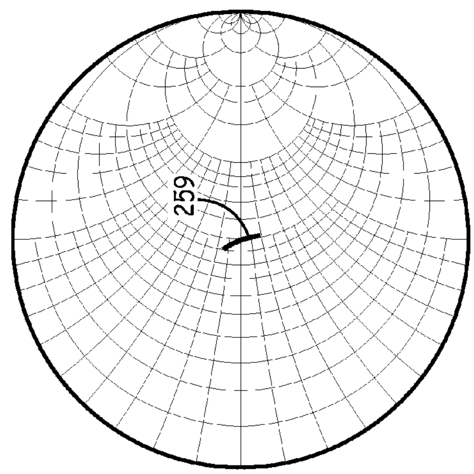


FIG. 8D

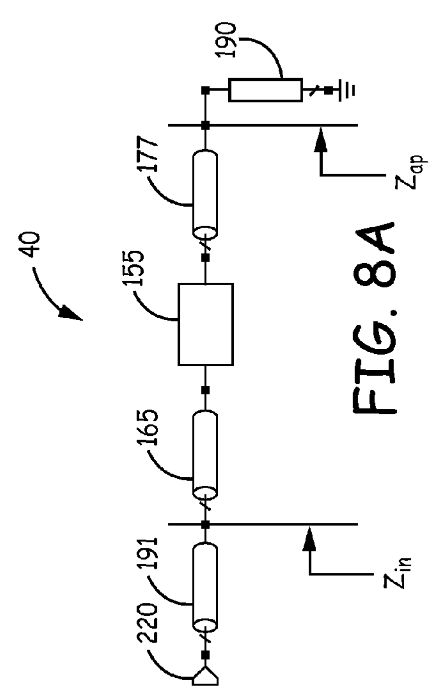


FIG. 8A

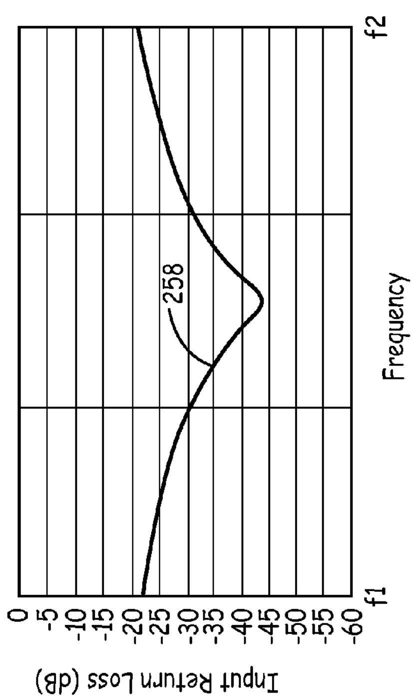


FIG. 8C

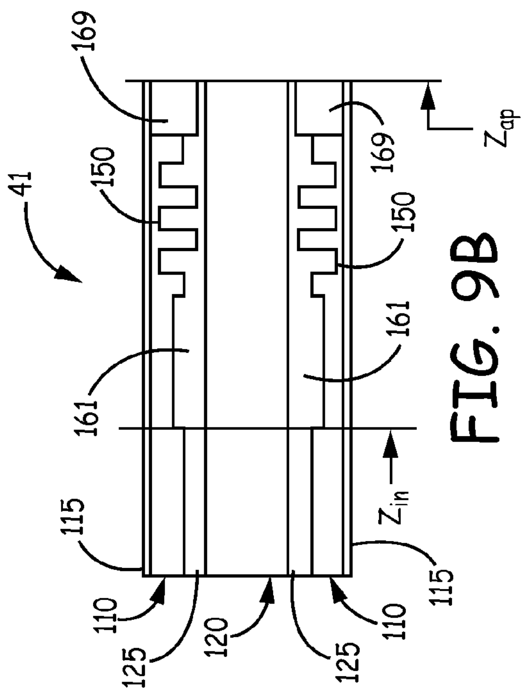


FIG. 9B

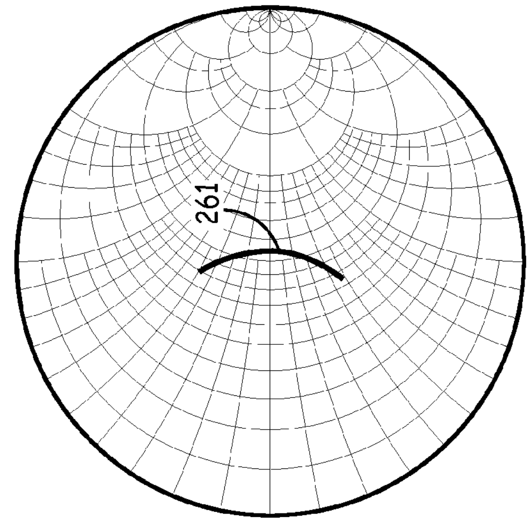


FIG. 9D

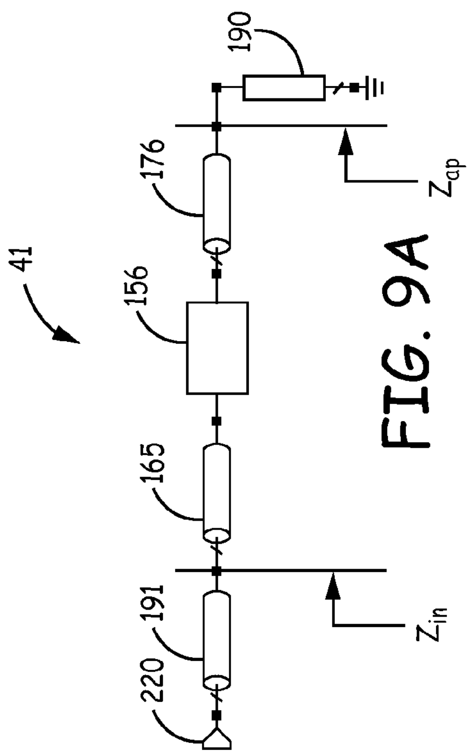


FIG. 9A

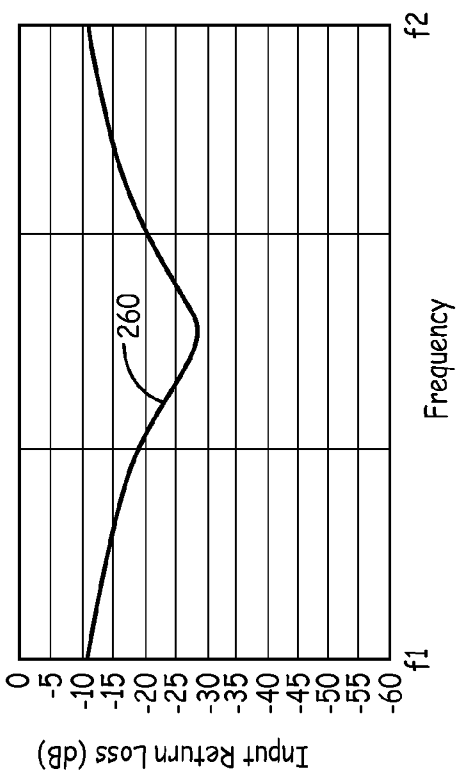


FIG. 9C

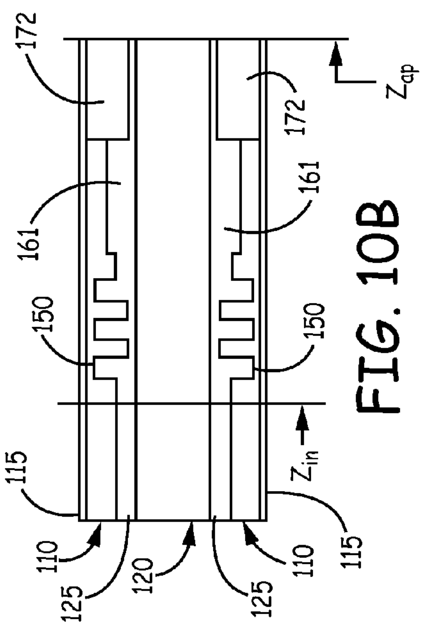


FIG. 10B

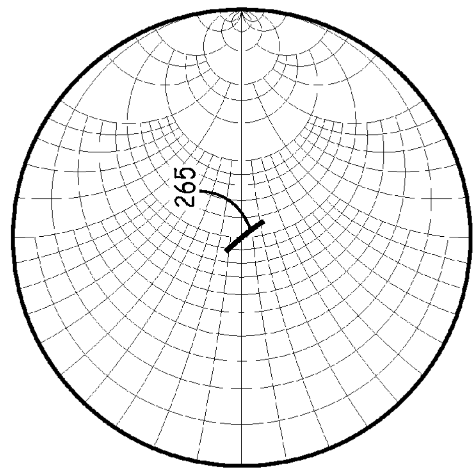


FIG. 10D

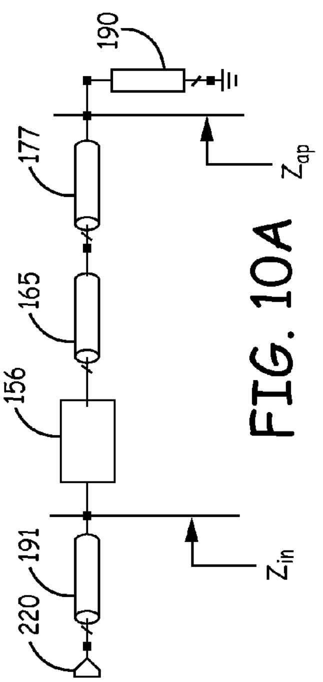


FIG. 10A

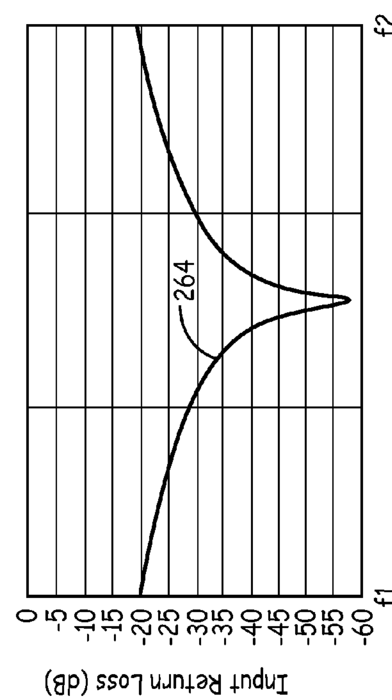


FIG. 10C

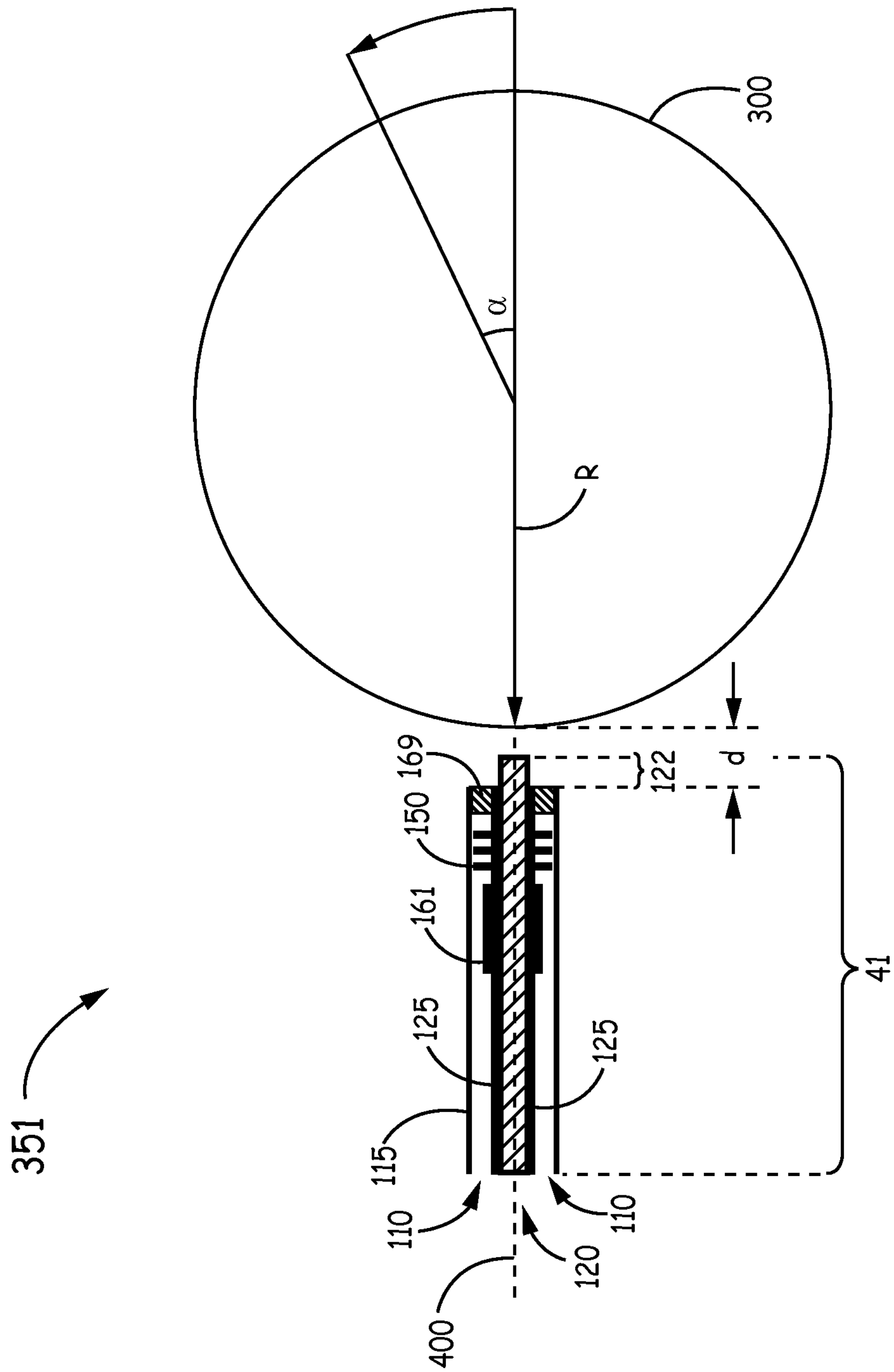
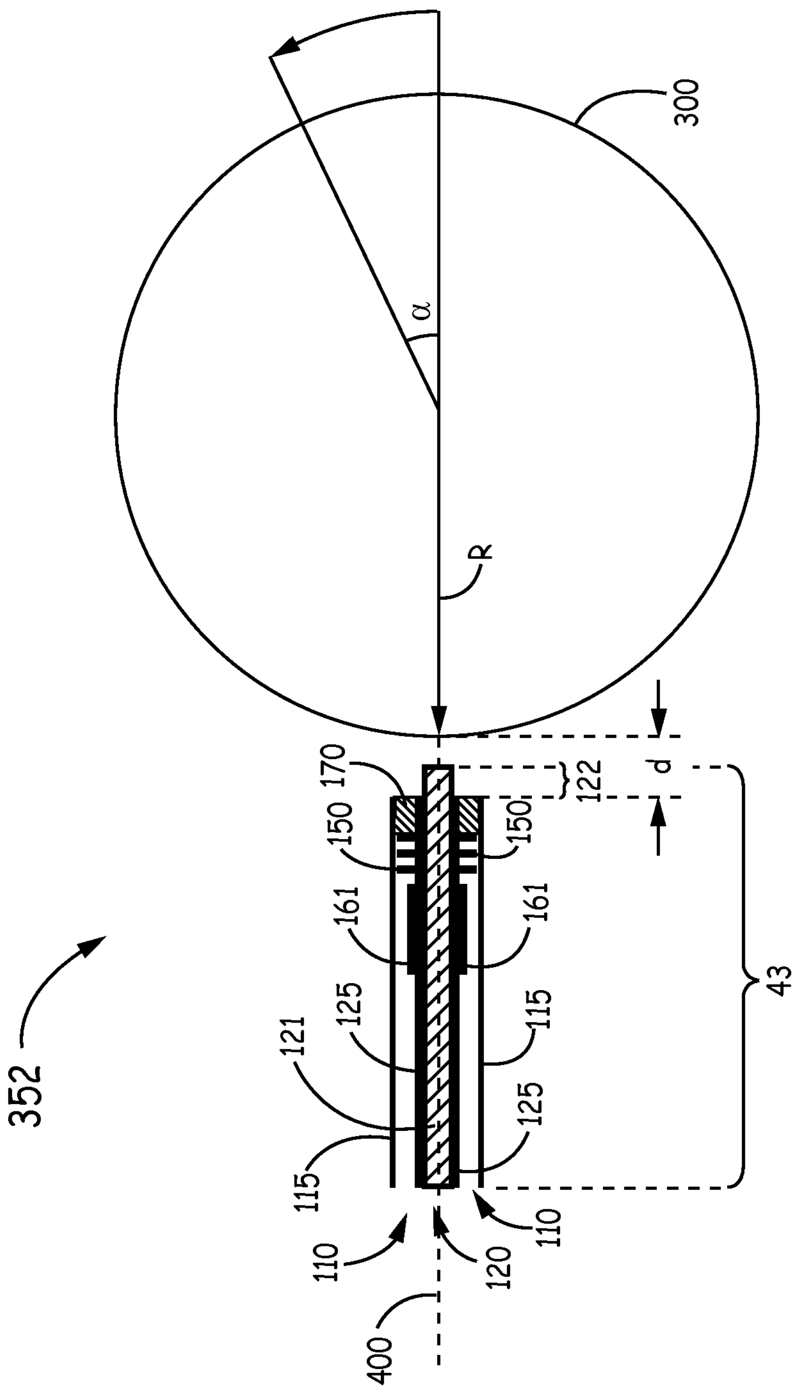


FIG. 11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352

FIG. 12

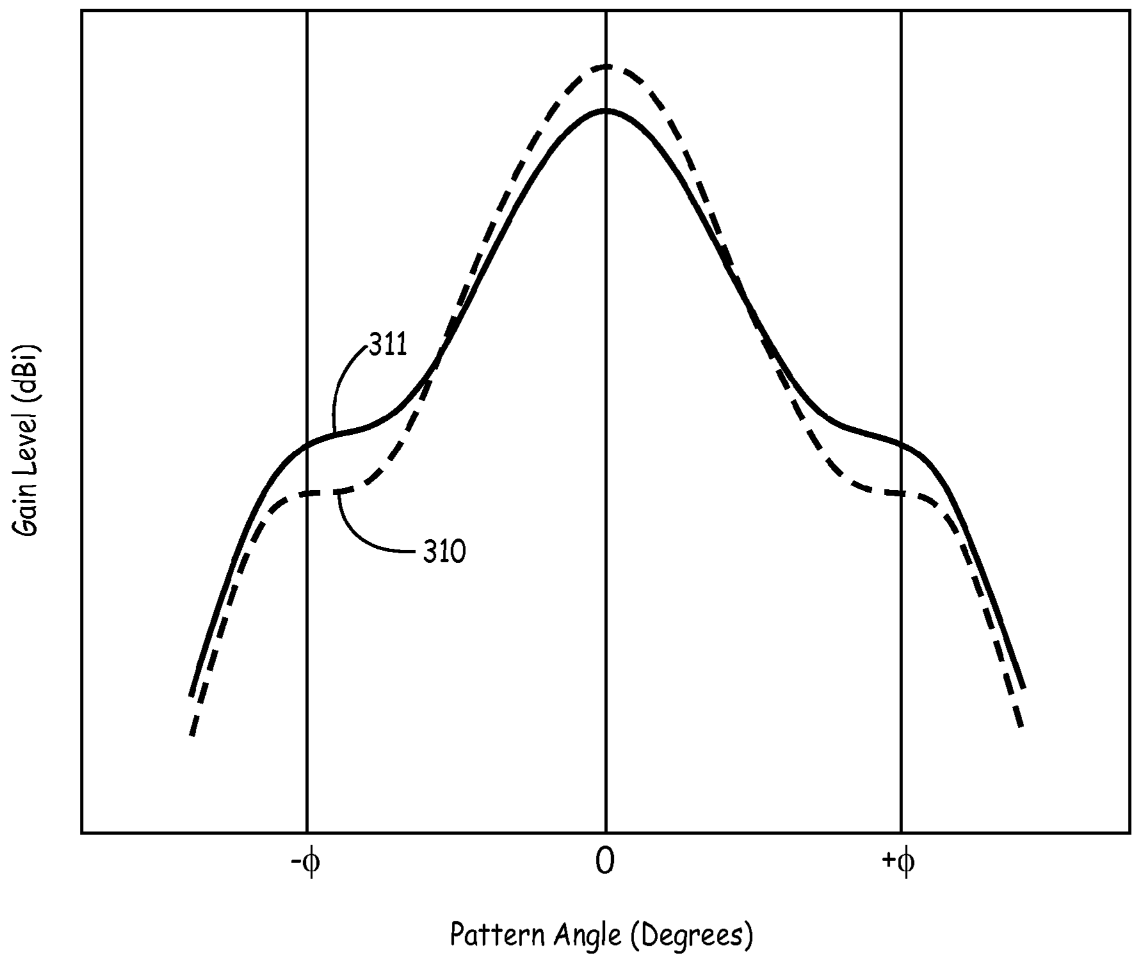
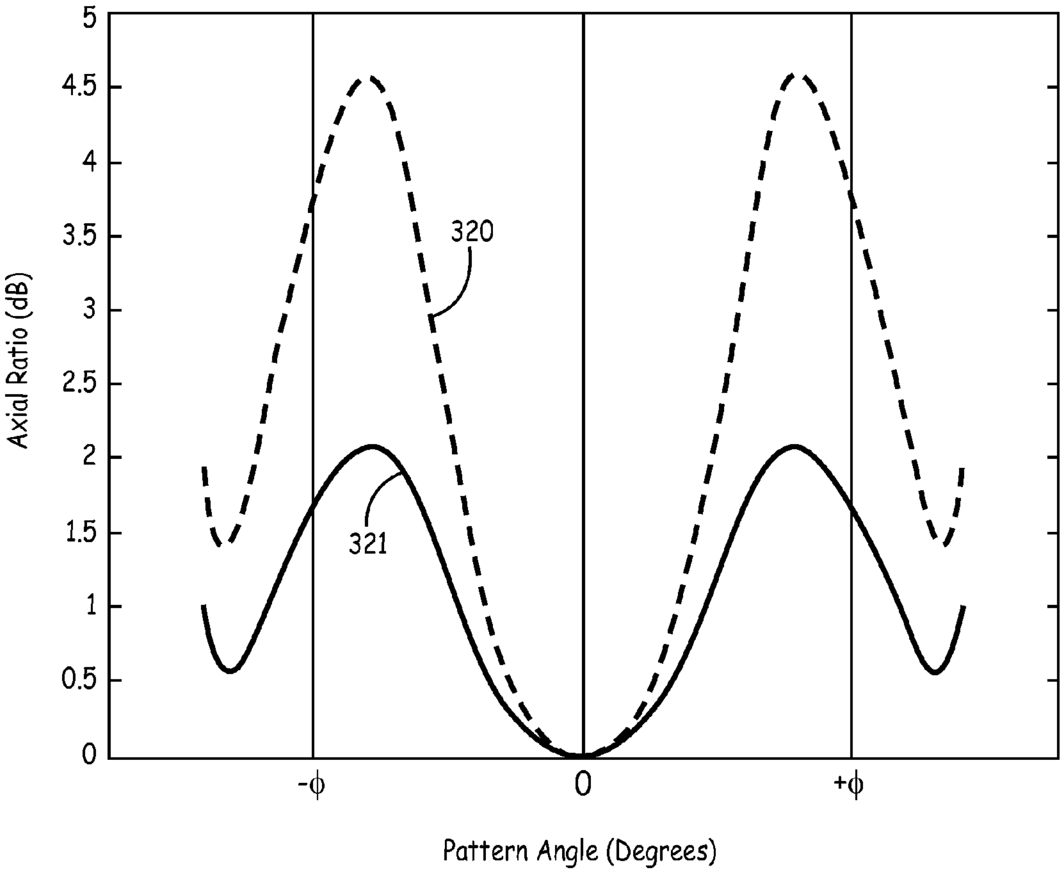


FIG. 13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4
3.5
3
2.5
2
1.5
1
0.5
0
Axial Ratio (dB)
320
321
-ϕ
0
+ϕ
Pattern Angle (Degrees)

FIG. 14

MATCHING AND PATTERN CONTROL FOR DUAL BAND CONCENTRIC ANTENNA FEED

This invention was made with support under Government Contract No. H94003-04-D0005 awarded by the US Government to Northrop Grumman. The US Government may have certain rights in the invention.

BACKGROUND

In currently available multi-band antenna feeds that use concentrically positioned coaxial and circular waveguide structures, the coaxial aperture is physically large or flares out to a diameter that is larger than that of the coaxial waveguide. This increased aperture size compared to the wavelength of operation facilitates the impedance matching of the waveguide to the free space impedance. However, while these physically-large antenna feeds may be useful as single feed elements, they are too large for a plurality of such feeds to be positioned around a common spherical dielectric lens for use in switched beam antenna systems. A compact form factor for a dual band concentric antenna feed having coaxial and circular waveguides is needed in order for multiple feeds to be operably positioned around a common lens.

SUMMARY

The present application relates to a dual band concentric antenna feed. The dual band concentric antenna feed includes an outer conductive tube having an inner surface and an inner conductive tube having an outer surface. The inner conductive tube is positioned inside the outer conductive tube and is coaxially aligned to a shared axis that extends a length of the outer conductive tube and the inner conductive tube. A coaxial waveguide formed in a space between the inner surface of the outer conductive tube and the outer surface of the inner conductive tube supports a first frequency band. A circular waveguide formed within an inner surface of the inner conductive tube supports a second frequency band. The dual band concentric antenna feed also includes at least one transformer, a filter, and a plug in the coaxial waveguide. The filter is offset from the at least one transformer. An impedance locus associated with the filter is high-frequency capacitive within the first frequency band and low-frequency inductive within the first frequency band. The plug is offset from the at least one transformer and the filter and positioned near an aperture end of the concentric antenna feed.

DRAWINGS

Understanding that the drawings depict only exemplary embodiments and are not therefore to be considered limiting in scope, the exemplary embodiments will be described with additional specificity and detail through the use of the accompanying drawings, in which:

FIG. **1** is a three-dimensional cut-away cross-section view of an embodiment of a dual band concentric antenna feed;

FIG. **2**A is a cross-section side view of the dual band concentric antenna feed of FIG. **1**;

FIG. **2**B is a cross-section side view of an embodiment of a dual band concentric antenna feed;

FIG. **3**A is a circuit model for a coaxial filter;

FIG. **3**B is a physical model of the coaxial filter of FIG. **3**A;

FIG. **3**C is a plot of the return loss of the coaxial filter of FIG. **3**A;

FIG. **3**D is a Smith chart showing the input impedance of the filter of FIG. **3**A;

FIG. **4** is a plot of the insertion loss of the coaxial filter of FIG. **3**A over a wide band of frequencies;

FIG. **5**A is a first-band circuit model of a dual band concentric antenna feed including a plug and a transformer in series;

FIG. **5**B is a physical model of a dual band concentric antenna feed including a plug and a transformer in series corresponding to the first-band circuit model of FIG. **5**A;

FIG. **5**C is a plot of the first-band return loss of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **5**A;

FIG. **5**D is a Smith chart showing the first-band input impedance of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **5**A;

FIG. **6**A is a first-band circuit model of a dual band concentric antenna feed including a plug and a two-stage transformer in series;

FIG. **6**B is a physical model of a dual band concentric antenna feed including a plug and a two-stage transformer in series corresponding to the first-band circuit model of FIG. **6**A;

FIG. **6**C is a plot of the first-band return loss of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **6**A;

FIG. **6**D is a Smith chart showing the first-band input impedance of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **6**A;

FIG. **7**A is a first-band circuit model of a dual band concentric antenna feed including a plug, a two-stage transformer, and a filter in series;

FIG. **7**B is a physical model of the dual band concentric antenna feed including a plug, a two-stage transformer, and a filter in series corresponding to the first-band circuit model of FIG. **7**A;

FIG. **7**C is a plot of the first-band return loss of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **7**A;

FIG. **7**D is a Smith chart showing the first-band input impedance of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **7**A;

FIG. **8**A is a first-band circuit model of a dual band concentric antenna feed including a plug (90 electrical degrees), a filter, and a transformer in series;

FIG. **8**B is a physical model of a dual band concentric antenna feed including a plug (90 electrical degrees), a filter, and a transformer in series corresponding to the first-band circuit model of FIG. **8**A;

FIG. **8**C is a plot of the first-band return loss of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **8**A;

FIG. **8**D is a Smith chart showing the input impedance of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **8**A;

FIG. **9**A is a first-band circuit model of a dual band concentric antenna feed including a plug (40 electrical degrees), a filter, and a transformer in series;

FIG. **9**B is a physical model of a dual band concentric antenna feed including a plug (40 electrical degrees), a filter, and a transformer in series corresponding to the first-band circuit model of FIG. **9**A;

FIG. **9**C is a plot of the first-band return loss of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **9**A;

FIG. **9**D is a Smith chart showing the first-band input impedance of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **9**A;

FIG. **10**A is a first-band circuit model of a dual band concentric antenna feed including a plug (90 electrical degrees), a transformer, and a filter in series;

FIG. **10**B is a physical model of a dual band concentric antenna feed including a plug (90 electrical degrees), a transformer, and a filter corresponding to the first-band circuit model of FIG. **10**A;

FIG. **10**C is a plot of the first-band return loss of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **10**A;

FIG. **10**D is a Smith chart showing the first-band input impedance of the dual band concentric antenna feed calculated from the first-band circuit model of FIG. **10**A;

FIGS. **11** and **12** are cross-sectional side views of dual band concentric feeds arranged with a lens;

FIG. **13** shows plots of the second-band antenna gain pattern for the dual band concentric feed and lens of FIG. **11** and FIG. **12**; and

FIG. **14** shows plots of the second-band axial ratio for the dual band concentric feed and lens of FIG. **11** and FIG. **12**.

In accordance with common practice, the various described features are not drawn to scale but are drawn to emphasize features relevant to the present invention. Like reference characters denote like elements throughout figures and text.

DETAILED DESCRIPTION

In the following detailed description, reference is made to the accompanying drawings that form a part hereof, and in which is shown by way of illustration specific illustrative embodiments in which the invention may be practiced. These embodiments are described in sufficient detail to enable those skilled in the art to practice the invention, and it is to be understood that other embodiments may be utilized and that logical, mechanical and electrical changes may be made without departing from the scope of the present invention. The following detailed description is, therefore, not to be taken in a limiting sense.

In order to overcome the problem described above, there is a need for special techniques to impedance match the coaxial aperture without increasing its size in a first frequency band. Additionally, a desire exists for methods which enable the gain pattern of the compact dual band concentric feed and lens antenna to be properly shaped in a second frequency band.

This application provides impedance matching in a first frequency band for a coaxial radiating element and a second frequency band with power radiating from the output of a circular waveguide of the dual band concentric antenna feed. The application also enables the antenna pattern in the second frequency band to be optimized for pattern shape and axial ratio. The dual band concentric antenna feeds described herein have a compact form factor so that multiple feeds can fit around a common lens. The compact dual band concentric antenna feeds described herein overcome the difficulty of prior art dual band concentric antenna feeds in providing impedance matching of the first frequency band at the coaxial aperture of the dual band concentric antenna feed and in optimizing the antenna pattern of the radiator for the second frequency band.

FIG. **1** is a three-dimensional cut-away cross-section view of an embodiment of a dual band concentric antenna feed **10**. FIG. **2**A is a cross-section side view of the dual band concentric antenna feed **10** of FIG. **1**. The dual band concentric antenna feed **10** includes an outer conductive tube **115** having an inner surface **116**, an inner conductive tube **125** having an outer surface **127**. The inner conductive tube **125** is positioned inside the outer conductive tube **115**. The inner conductive tube **125** and the outer conductive tube **115** are coaxially aligned to a shared axis **400** (FIG. **2**A) that extends a length (in the Z direction) of the outer conductive tube **115** and the inner conductive tube **125**. The shared axis **400** is parallel to the Z_{out} axis shown in FIGS. **1** and **2**A. The outer conductive tube **115** has a cylindrical shape. An inner surface **126** of the inner conductive tube **125** is a smooth cylindrical shape.

A coaxial waveguide **110** is formed in a space between the inner surface **116** of the outer conductive tube **115** and the outer surface **127** of the inner conductive tube **125** and supports a first frequency band. A circular waveguide **120** is formed within an inner surface **126** of the inner conductive tube **125** and supports a second frequency band.

The dual band concentric antenna feed **10** also includes at least one transformer in the coaxial waveguide **110**, a filter **150** in the coaxial waveguide **110**, and a plug **170** in the coaxial waveguide **110**. As shown in FIGS. **1** and **2**A, the at least one transformer includes a first transformer **161** and a second transformer **162**. The filter **150** is offset from the first transformer **161** and the second transformer **162**. The plug **170** is offset from the first transformer **161**, the second transformer **162**, and the filter **150**. The plug **170** is positioned at or near (e.g., within in millimeters) an aperture end represented generally at **180** of the concentric antenna feed **10**. The output end **180** is also referred to herein as an "aperture end **180**". The output end **180** of the dual band concentric antenna feed **10** spans an output plane (X_{out}, Y_{out}). The output plane (X_{out}, Y_{out}) is also referred to herein as an "aperture plane (X_{out}, Y_{out})".

The first transformer **161**, the second transformer **162**, and the filter **150** are formed in the coaxial waveguide **110** to provide impedance matching for the dual band concentric antenna feed **10** in a first frequency band. As understood by one skilled in the art, as the return loss of a dual band concentric antenna feed decreases, the impedance of the dual band concentric antenna feed is better matched to the characteristic impedance of the input transmission line **191**.

The plug **170** is formed in (fills) the space between the outer surface **127** of the inner conductive tube **125** and the inner surface **116** of the outer conductive tube **115** at the coaxial aperture in the plane (X_{out}, Y_{out}) of the dual band concentric antenna feed **10**. The plug **170** has a plug length L_p in the −Z direction from the aperture plane (X_{out}, Y_{out}). In the embodiment of FIGS. **1** and **2**A, the plug length L_p is approximately 90 electrical degrees in the first frequency band. A plug length L_p of approximately 90 electrical degrees is equivalent to a quarter of a guide wavelength ($\lambda_g/4$) at the mid-frequency, which equals $(f_1+f_2)/2$. All references to 90 electrical degrees are referred to the mid-frequency. Likewise, all references to 40 electrical degrees are referred to the mid-frequency. The plug **170** is formed from a dielectric material.

As shown in FIGS. **1** and **2**A, the outer surface **127** of the inner conductive tube **125** includes ribbed protrusions represented generally at **150**. These ribbed protrusions change the transmission properties of the coaxial waveguide **110** in the region of the protrusions to achieve the desired filtering and impedance matching functions of the filter. The region of the ribbed protrusions is referred to herein as a "filter **150**", a "coaxial filter **150**", or a "filter/matching element **150**". The filter **150** is used to improve the impedance matching of the dual band concentric antenna feed **10** in a first frequency band. In one implementation of this embodiment, the filter **150** is formed from the conductive material that forms the inner conductive tube **125**. In another implementation of this embodiment, the filter includes rings that are arranged in the coaxial waveguide **110** of the inner conductive tube **125**. Such rings are made from conductive material. In yet another embodiment, the rings are formed from the same metal as the inner conductive tube **125**.

As shown in FIGS. **1** and **2**A, the inner conductive tube **125** also includes a ring of material **161** and a protrusion **162**. The protrusion **162** encircles the inner conductive tube **125** and is formed from the conductive material that forms the inner conductive tube **125**. The ring of material **161** changes the characteristic impedance of the coaxial waveguide **110** in the region of the ring of material **161** to achieve the desired characteristic impedance of a first transformer. The region of the ring of material **161** is referred to herein as the "ring of material **161**", "dielectric ring **161**", a "first transformer stage **161**", "first transformer **161**" and "transformer **161**".

Likewise, the protrusion **162** of the outer surface **127** of the inner conductive tube **125** changes the characteristic impedance of the coaxial waveguide **110** in the region of the protrusion **162** to achieve the desired characteristic impedance of a second transformer. The region of the protrusion **162** is referred to herein as a "second transformer stage **162**" and "second transformer **162**". As shown in FIG. **2**A, there is an air gap **128** between the second transformer **162** and the inner surface **116** of the outer conductive tube **115**. The terms "gap" and "air gap" are used interchangeably herein.

In one implementation of this embodiment, the first transformer **161** comprises a dielectric ring **161**. As shown in FIG. **2**A, the dielectric ring **161** contacts the inner surface **116** of the outer conductive tube **115**. In another implementation of this embodiment, a negligible gap (on the order of one or two mils) exists between the inner surface **116** of the outer conductive tube **115** and the dielectric ring **161**.

FIG. **2**B is a cross-section side view of a dual band concentric antenna feed **9**. The dual band concentric antenna feed **9** differs from the dual band concentric antenna feed **10** of FIGS. **1** and **2**A, in that there is an air gap **129** between the first transformer **159** and the inner surface **116** of the outer conductive tube **115**. The air gap **129** is also referred to herein as a "first air gap **129**" and "first gap **129**". The air gap **128** is also referred to herein as a "second air gap **128**" and "second gap **128**".

In one implementation of this embodiment, the first transformer **159** is formed in the coaxial waveguide **110** as a first protrusion **159** on the outer surface **127** of the inner conductive tube **125** and the second transformer **162** is formed in the coaxial waveguide **110** as a second protrusion **162** on the outer surface **127** of the inner conductive tube **125**. In such an embodiment, the first protrusion **159** and the second protrusion **162** have different thicknesses and they are seamlessly formed on the outer surface **127** of the inner conductive tube **125**. In this embodiment, the first gap **129** is between the first protrusion **129** and the inner surface **116** of the outer conductive tube **115**, and the second gap **128** is between the second protrusion **162** and the inner surface **116** of the outer conductive tube **115**.

In another implementation of this embodiment, the first transformer **159** is a ring of dielectric material **159**. In yet another implementation of this embodiment, the first transformer **159** is a ring of conductive material **159**. Hereafter, a reference to the dual band concentric antenna feed **10** can also be applied to the dual band concentric antenna feed **9** of FIG. **2**B, as is understandable to one skilled in the art upon reading this document.

The dual band concentric antenna feed **10** includes a coaxial waveguide **110** formed in the space between the outer surface **127** of the inner conductive tube **125** and the inner surface **116** of the outer conductive tube **115**. The coaxial waveguide **110** is configured to support the propagation of electromagnetic fields at a first band of frequencies. The dual band concentric antenna feed **10** also includes a circular waveguide **120** formed inside the inner conductive tube **125**. The circular waveguide **120** is configured to support propagation of electromagnetic fields at a second band of frequencies. The first band of frequencies is also referred to herein as "band 1" or "first band". The second band of frequencies is also referred to herein as "band 2" or "second band". The second band of frequencies is at a higher frequency than the first band of frequencies. In the transmit case, the electromagnetic fields propagate from an input end represented generally at **181** to the output end **180** at the output plane (X_{out}, Y_{out}). The output end **180** at the output plane (X_{out}, Y_{out}) is offset from the plane of the input end **181** by a length L_{dbc} (FIG. **2**A) of the dual band concentric antenna feed **10**. In the receive case, the electromagnetic fields propagate in the opposite direction within the dual band concentric antenna feed **10** from the output end **180** toward the input end **181**.

As shown in FIGS. **1** and **2**A, the inner conductive tube **125** is filled with a dielectric material **121** that is selected to lower the cutoff frequency of the circular waveguide **120** so that electromagnetic waves in the second frequency band propagate within the inner conductive tube **125**. As known to those skilled in the art, use of dielectric material **121** allows the diameter of circular waveguide **120** (e.g., the inner diameter of the inner conductive tube **125**) to be reduced. In one implementation of this embodiment, the inner conductive tube **125** is filled with air rather than the dielectric material **121**.

In one implementation of this embodiment, the inner conductive tube **125** is formed in aluminum. In another implementation of this embodiment, the outer conductive tube **115** is formed in aluminum. In yet another implementation of this embodiment, the inner conductive tube **125** is formed in other metals. In yet another implementation of this embodiment, the outer conductive tube **115** is formed in in other metals.

The first transformer **161** and the second transformer **162** are constructed of dielectric rings and/or metal sections of varying diameters. The design of the first transformer **161** and the second transformer **162** depends upon the available room within the dual band concentric antenna feed **10**. In one implementation of this embodiment, the first transformer **161** is a dielectric ring and the second transformer **162** is formed as a protrusion in the coaxial waveguide **110** (FIGS. **1** and **2**A) of the inner conductive tube **125**. There are various ways to achieve the desired characteristic impedance of a given transformer in the coaxial feed.

In one implementation of this embodiment, there is a step-out in the outer diameter of inner conductive tube **125** in the second transformer region to form the second transformer **162** so the second transformer **162** is a protrusion of the inner conductive tube **125**. A dielectric ring having a specific dielectric constant is positioned adjacent to the step-out forms the first transformer **161** and completely fills the space between inner conductive tube **125** and outer conductive tube **115** (FIG. **2**A).

In another implementation of this embodiment, the second transformer **162** is a protrusion of the inner conductive tube **125**. The first transformer **159** is formed by partially filling the coaxial waveguide with a dielectric ring **159** (FIG. **2**B) between outer surface **127** of the inner conductive tube **125** and outer conductive tube **115**. In this case there is an air gap **129** between dielectric ring **159** and outer conductive tube **115**.

In theory, the physical configurations of the first transformer **161** and the second transformer **162** are designed independently according to the embodiments described above. Thus, there are many conceivable combinations of the embodiments for the first transformer **161** and the second transformer **162** taken together. In practice, the first transformer **161** and the second transformer **162** must have physical designs that are compatible for practical assembly of the piece parts. For example, if a dielectric ring is used for the second transformer **162**, the dielectric ring must be able to slide past any protrusion that comprises the first transformer **161**. In one embodiment, the first transformer **161** and the second transformer **162** are formed from dielectric rings with the same or different inner diameter and with the same or different outer diameter. In this latter case, the first transformer **161** and the second transformer **162** are made as one piece part. In yet another embodiment, the first transformer **161** and the second transformer **162** are formed from dielectric rings and are made as part of the same piece part as plug **170**.

The shape of the filter **150**, the plug **170**, the first transformer stage **161**, and the second transformer stage **162** and the dielectric constant of the plug **170** and first transformer stage **161** are determined by modeling. The modeling techniques are now described with reference to FIGS. **3**A-**3**D and **5**A-**10**D.

FIG. **3**A is a circuit model for a coaxial filter **155**, which is illustrated as a generic two port network. The circuit model for the coaxial filter **155** includes an input port **220** and an output port **221** that are separated by the length between points **1** and **2**. FIG. **3**B is a physical model of the coaxial filter **155** of FIG. **3**A. The circuit model of the coaxial filter **155** of FIG. **3**A represents physical model filter **150**. The filter **150** of FIG. **3**B includes an input port **151** that corresponds to the input port **220** of the circuit model of FIG. **3**A and an output port **152** that corresponds to the output port **221** of the circuit model of FIG. **3**A.

FIG. **3**C is a plot **250** of the return loss of the coaxial filter **155** of FIG. **3**A. Plot **250** spans the frequency range for the first band of frequencies (i.e., between frequency f_1 and frequency f_2). As shown in FIG. **3**C, at the edges of the first band (i.e., near frequency f_1 and near frequency f_2), the return loss is at or less than −25 dB. FIG. **3**D is a Smith chart showing the input impedance of the filter **155** of FIG. **3**A. The real axis of the Smith chart is the horizontal line that bisects the Smith chart. Each plot on the Smith charts shown in FIGS. **3**D, **5**D, **6**D, **7**D, **8**D, **9**D, and **10**D is referred to herein as an "impedance locus". The impedance locus **251** shown on the Smith chart of FIG. **3**D, shows that the impedance is inductive at frequency f_1 (i.e., above the real axis) and the impedance is capacitive at frequency f_2 (i.e., below the real axis). The impedance locus **251** depicts the input impedance of input port **220** of coaxial filter **155** with the output port **221** match terminated. At a frequency approximately midway between f_1 and f_2, the impedance locus passes through the center of the Smith chart indicating a near perfect impedance match. Thus, the coaxial filter **155** is high-frequency (e.g., frequency f_2) capacitive within the first frequency band (e.g., from f_1 and f_2) and is low-frequency (e.g., frequency f_1) inductive within the first frequency band. The relative short length of the impedance locus **251** near the center of the Smith chart indicates that the impedance is relatively well matched from frequency f_1 to frequency f_2.

FIG. **4** is a plot of the insertion loss of the coaxial filter **155** of FIG. **3**A over a wide band of frequencies. The first band of frequencies from frequency f_1 to frequency f_2 is represented generally at **231**. The second band of frequencies is represented generally at **232** and includes the frequencies above the frequency f_3. As shown in FIG. **4**, the filter **150** is a low-pass filter since it "passes" band 1 energy (first band **231** of frequencies) and rejects, to better than −40 dB, the frequencies in band 2 (second band **232** of frequencies) above frequency f_3. The −40 dB rejection in band 2 is from input port **220** to the output port **221** (and vice versa) in FIG. **3**A.

In the following description related to FIGS. **5**A-**10**D, FIGS. **5**A, **6**A, **7**A, **8**A, **9**A, and **10**A show circuit models for respective coaxial waveguide feeds of the dual band concentric antenna feeds of FIGS. **5**B, **6**B, **7**B, **8**B, **9**B, and **10**B. A coaxial waveguide feed is the coaxial component of a dual band concentric antenna feed, as known to one skilled in the art. Likewise, FIGS. **5**C, **6**C, **7**C, **8**C, **9**C, and **10**C show the return loss for the respective coaxial waveguide feeds of the dual band concentric antenna feeds of FIGS. **5**B, **6**B, **7**B, **8**B, **9**B, and **10**B. FIGS. **5**D, **6**D, **7**D, **8**D, **9**D, and **10**D show the Smith charts for the respective coaxial waveguide feeds of the dual band concentric antenna feeds of FIGS. **5**B, **6**B, **7**B, **8**B, **9**B, and **10**B. However, to simplify the description, it is understood to those skilled in the art that the term "dual band concentric antenna feed" may be used in place of "coaxial waveguide feed of the dual band concentric antenna feed" when referring to FIGS. **5**A, **6**A, **7**A, **8**A, **9**A, **10**A, **5**C, **6**C, **7**C, **8**C, **9**C, **10**C, **5**D, **6**D, **7**D, **8**D, **9**D, and **10**D. Said differently, it is implied that the results refer to the coaxial waveguide feed of the dual band concentric antenna feed and not the circular waveguide feed of the dual band concentric antenna feed (even if the term "coaxial" is not mentioned) when referring to FIGS. **5**A, **6**A, **7**A, **8**A, **9**A, **10**A, **5**C, **6**C, **7**C, **8**C, **9**C, **10**C, **5**D, **6**D, **7**D, **8**D, **9**D, and **10**D.

FIG. **5**A is a first-band circuit model for a dual band concentric antenna feed having a plug **175** and a transformer **165** in series. FIG. **5**B is a physical model of the dual band concentric feed having a plug **170** and transformer **161** in series. The components **191**, **165**, and **175** in the circuit model of FIG. **5**A are transmission line circuit elements which correspond to sections of the physical coaxial feed model of FIG. **5**B. Each transmission line circuit element is represented by its own characteristic impedance, propagation constant, and physical length. In the circuit model, the propagation constant and the physical length are replaced by an equivalent electrical length at a specified frequency usually chosen to be the arithmetic mean of f_1 and f_2. The TE_{11} mode is the desired mode of electromagnetic wave propagation in the coaxial feed and all characteristic impedances are calculated with respect to this mode. The plug **175** and transformer **165** are in series with an input transmission line **191**, which has the same characteristic impedance as the input port **220**. These transmission line circuit elements **191**, **165**, and **175** lead to and feed the parallel aperture impedance **190** (Z_{ap}) of the coaxial aperture in the output plane (X_{out}, Y_{out}). The parallel aperture impedance **190** (Z_{ap}) at the aperture (output) plane is also referred to herein as a "shunt coaxial aperture impedance **190**". As shown in FIG. **5**A, the input impedance of the feed (Z_{in}) is defined as the impedance terminating the input transmission line **191**; i.e., it is the impedance as observed looking into the equivalent circuit of the transformer **165**, the plug **175**, and the shunt coaxial aperture impedance **190**.

The circuit model of the plug **175** of FIG. **5**A represents the physical model of the plug **170** of FIG. **5**B. Likewise, the circuit model of transformer **165** of FIG. **5**A represents the physical model transformer **161** of FIG. **5**B. The serially arranged plug **170** and the transformer **161** of FIG. **5**B form a dual band concentric antenna feed **20**. The reference plane for the input impedance (Z_{in}) in FIG. **5**B correlates to the reference plane for the input impedance (Z_{in}) in FIG. **5**A. The reference plane for the aperture impedance (Z_{ap}) in FIG. **5**B correlates to the reference plane for the aperture impedance **190** in FIG. **5**A. FIG. **5**C is a plot of the return loss **252** of the coaxial feed circuit model of FIG. **5**A with respect to the input port **220**. As shown in FIG. **5**C, at the edges of the first band (i.e., near frequency f_1 and near frequency f_2), the return loss is at or less than −25 dB. FIG. **5**D is a Smith chart showing the input impedance (Z_{in}) of the circuit model of FIG. **5**A. The relative short length of the impedance locus **253** indicates that the impedance is relatively well matched from frequency f_1 to frequency f_2. The impedance locus **253** shown on the Smith chart of FIG. **5**D, shows that the impedance is inductive at frequency f_1 and the impedance is capacitive at frequency f_2. With a single transformer **161**, the coaxial aperture is well-matched, and is low-frequency (f_1) inductive and high frequency (f_2) capacitive. This is similar to the filter impedance locus shown in FIG. **3**D for filter **150**.

FIG. **6**A is a first-band circuit model for a dual band concentric antenna feed having a plug **175** and a two-stage transformer **165** and **166** in series. FIG. **6**B is a physical model of the dual band concentric antenna feed **21** having the plug **175** and the two-stage transformer **165** and **166** of FIG. **6**A. The components **191**, **166**, **165**, and **175** in the circuit model of FIG. **5**A are transmission line circuit elements which correspond to sections of the physical coaxial feed model of FIG. **6**B. Each transmission line circuit element is represented by its own characteristic impedance, propagation constant, and physical length. In the circuit model, the propagation constant and the physical length are replaced by an equivalent electrical length at a specified frequency usually chosen to be the arithmetic mean of f_1 and f_2. The TE_{11} mode is the desired mode of electromagnetic wave propagation in the coaxial feed and all characteristic impedances are calculated with respect to this mode. The plug **175**, the first transformer **165**, and the second transformer **166** are in series with an input transmission line **191**, which has the same characteristic impedance as the input port **220**. These transmission line circuit elements **191**, **165**, **166**, and **175** lead to and feed the parallel aperture impedance **190** (Z_{ap}) at the aperture (output) plane (X_{out}, Y_{out}). The parallel aperture impedance **190** (Z_{ap}) of the coaxial aperture in the output plane is also referred to herein as a "shunt coaxial aperture impedance **190**". As shown in FIG. **6**A, the input impedance of the feed (Z_{in}) is defined as the impedance terminating the input transmission line **191**; i.e., it is the impedance as observed looking into the equivalent circuit of the second transformer **166**, the first transformer **165**, the plug **175**, and the shunt coaxial aperture impedance **190**.

The circuit model of the plug **175** of FIG. **6**A represents the plug **170** of FIG. **6**B. Likewise, the circuit model of first transformer **165** of FIG. **6**A represents the physical model of the first transformer **161** of FIG. **6**B and the circuit model of second transformer **166** of FIG. **6**A represents the physical model of the second transformer **162** of FIG. **6**B.

The reference plane for the input impedance (Z_{in}) in FIG. **6**B correlates to the reference plane for the input impedance (Z_{in}) in FIG. **6**A. The plug **170**, the first transformer **161**, and the second transformer **162** of FIG. **6**B in series form the coaxial portion of the dual band antenna feed **21**. The plug **170** has a length of approximately 90 electrical degrees in the first frequency band (i.e., at $f_{mid}=(f_1+f_2)/2$).

FIG. **6**C is a plot **254** of the return loss referenced to input port **220** of the coaxial feed circuit model of FIG. **6**A having plug **175** and the two-stage transformer **165** and **166**. As shown in FIG. **6**C, at the edges of the first band (i.e., near frequency f_1 and near frequency f_2), the return loss is at or less than −25 dB. FIG. **6**D is a Smith chart showing the input impedance (Z_{in}) of the coaxial feed of FIGS. **6**A and **6**B. The impedance locus **255** shown on the Smith chart of FIG. **6**D, shows that the impedance is high frequency (e.g., frequency f_2) inductive within the first frequency band (e.g., from f_1 to f_2) and the impedance is low frequency (e.g., frequency f_1) capacitive within the first frequency band. As shown in FIG. **6**D, the input impedance looking into the equivalent circuit of the second transformer **166**, the first transformer **165**, the plug **175**, and the shunt coaxial aperture impedance **190** is low-frequency capacitive in the first frequency band and is high-frequency inductive in the first frequency band. This differs from the impedance loci **251** and **253** of FIGS. **3**D and **5**D, respectively, in which the impedance is high-frequency (e.g., frequency f_2) capacitive within the first frequency band and is low-frequency (e.g., frequency f_1) inductive within the first frequency band.

FIG. **7**A is a first-band circuit model of the dual band concentric antenna feed **10** (FIGS. **1** and **2**A). The first-band circuit model of the dual band concentric antenna feed **10** includes a plug **175**, a two-stage transformer **165** and **166**, and a filter **155** in series. FIG. **7**B is a physical model of the dual band concentric antenna feed **10** corresponding to the circuit model of FIG. **7**A. FIG. **7**B differs from FIG. **6**B by the addition of a filter **150** to the dual band concentric antenna feed **21** of FIG. **6**B. The circuit model of the plug **175** of FIG. **7**A represents the physical model plug **170** of FIG. **7**B. The circuit model of first transformer **165** of FIG. **7**A represents the physical model of the first transformer **161** of FIG. **7**B and the circuit model of second transformer **166** of FIG. **7**A represents the physical model of the second transformer **162** of FIG. **7**B. The circuit model of filter **155** of FIG. **7**A represents the physical model of the filter **150** of FIG. **7**B. The plug **170**, the first transformer **161**, and the second transformer **162**, and filter **150** of FIG. **7**B in series form the dual band concentric antenna feed **10** shown in FIGS. **1** and **2**A. The first transformer **161** is positioned between the plug **170** and the second transformer **162**. The second transformer **162** is positioned between the filter **150** and the first transformer **161**.

FIG. **7**C is a plot **256** of the return loss of the dual band concentric antenna feed **10** of FIG. **7**A. As shown in FIG. **7**C, at the edges of the first band (i.e., near frequency f_1 and near frequency f_2), the return loss is at or less than −30 dB. FIG. **7**D is a Smith chart showing the input impedance in the first frequency band of the dual band concentric antenna feed **10** of FIG. **7**A. FIGS. **7**A-**7**D show a dual band concentric antenna feed in which the impedance of the filter counteracts the feed impedance of FIGS. **6**A-**6**D.

As shown in FIG. **7**D, the addition of the filter **150** to the dual band concentric antenna feed **21** of FIG. **6**B causes the impedance locus **257** of the Smith chart to collapse to almost a point and, thus, provides a return loss less than −30 dB over the band of interest (i.e., from f_1 to f_2). This collapse of the impedance locus **257** is produced by using the two transformers **161** and **162** (FIG. **6**B), which provide a feed input impedance that is low-frequency capacitive in the first frequency band and high-frequency inductive in the first frequency band, in series with the filter **150** (FIG. **3**), which has an impedance that is high-frequency capacitive in the first frequency band and low-frequency inductive in the first frequency band. The small diameter of the impedance locus **257** centered on the Smith chart indicates that the impedance (i.e., the shunt coaxial aperture impedance **190**) is well matched from frequency f_1 to frequency f_2. In this manner, good performance (e.g., very low input return loss and excellent impedance matching) is obtained for the dual band concentric antenna feed **10** in the first frequency band. Thus, the input impedance of the coaxial feed physically consisting of a plug

170, a two-stage transformer 161 and 162, and a filter 155 in series is very well matched across all of the first band 231 of frequencies from frequency f_1 to frequency f_2.

Another embodiment of a dual band concentric antenna feed improves the second-band antenna gain pattern when used with a lens and provides good, but not optimal, first-band impedance matching is shown in FIGS. 8A-8D. FIG. 8A is a first-band circuit model for the dual band concentric antenna feed having a plug 177 (90 electrical degrees), a filter 155, and a transformer 165 in series. The circuit model of the plug 177 of FIG. 8A represents the physical model of the plug 172 of FIG. 8B. The reference plane for the input impedance (Z_{in}) in FIG. 8B correlates to the reference plane for the input impedance (Z_{in}) in FIG. 8A. The plug 172 has a length of 90 electrical degrees in the first frequency band. The circuit model of filter 155 of FIG. 8A represents the physical model filter 150 of FIG. 8B. Likewise, the circuit model of transformer 165 of FIG. 8A represents the physical model transformer 161 of FIG. 8B. The plug 172, the filter 150, and the transformer 161 of FIG. 8B in series form a dual band concentric antenna feed 40. As shown in FIG. 8B, the filter 150 is positioned between the transformer 161 and the plug 172. The filter/matching element 150 is positioned directly, or almost directly, behind the plug 172. The matching transformer 161 is shown after the filter/matching element 150. FIG. 8C is a plot of the return loss of the dual band concentric antenna feed 40 of FIGS. 8A and 8B. As shown in FIG. 8C, at the edges of the first band (i.e., near frequency f_1 and near frequency f_2), the return loss is less than −20 dB. FIG. 8D is a Smith chart showing the input impedance of the dual band concentric antenna feed 40 of FIG. 8A. The relatively short length of the impedance locus 259 indicates that the impedance is relatively well matched.

FIG. 9A is a first-band circuit model of the dual band concentric antenna feed 41 having a plug 176, a filter 156, and a transformer 165 in series. FIG. 9B is a physical model of the dual band concentric antenna feed of FIG. 9A. The circuit model of the plug 176 of FIG. 9A represents the physical model of the plug 169 of FIG. 9B. The plug 169 has a length of 40 electrical degrees in the first frequency band. FIG. 9C is a plot of the return loss of the dual band concentric antenna feed of FIG. 9A. As shown in FIG. 9C, at the edges of the first band (i.e., near frequency f_1 and near frequency f_2), the return loss is at or less than −10 dB, which is relatively high compared to the return loss of the dual band concentric antenna feed 10 shown in FIG. 7C. FIG. 9D is a Smith chart showing the input impedance of the dual band concentric antenna feed of FIG. 9A. The relatively long length of the impedance locus 261 indicates that the impedance is not very well matched from frequency f_1 to frequency f_2. The relatively high return loss and mismatched impedance of the dual band concentric antenna feed 41 is due to the length of the plug 169 being significantly less than the optimal 90 degrees, e.g., 40 electrical degrees in this case. By decreasing the plug length from 90 electrical degrees in FIG. 8B to 40 electrical degrees in FIG. 9B, the return loss and the impedance locus in the dual band concentric antenna feed 41 is degraded from that of the dual band concentric antenna feed 40 of FIG. 8B. The input return loss and the impedance locus are significantly affected by the distance between the filter 150 and the output aperture of the dual band concentric antenna feed. This distance includes the plug length and any additional space between the plug 169 or 172 and the filter 150.

FIG. 10A is a first-band circuit model of the dual band concentric antenna feed having a plug 177 (90 electrical degrees in the first frequency band), a transformer 165, and a filter 156 in series. FIG. 10B is a physical model of the dual band concentric antenna feed 42 of FIG. 10A. FIG. 10C is a plot of the return loss of the dual band concentric antenna feed 42 of FIG. 10A. As shown in FIG. 10C, at the edges of the first band (i.e., near frequency f_1 and near frequency f_2), the return loss is approximately −20 dB. FIG. 10D is a Smith chart showing the input impedance of the dual band concentric antenna feed 42 of FIG. 10A.

One purpose of the filter/matching element 150 is to prevent electromagnetic waves in the second frequency band from propagating in the coaxial waveguide 110. A second function of the filter/matching element 150 is to provide optimal matching of the coaxial aperture in conjunction with two transformers as shown in FIGS. 7A and 7B. In some applications due to size or cost constraints, there is only one transformer in the dual band concentric feed design. In this case it is helpful to examine the effects on the location of a single transformer relative to the filter 150. This is done by comparing FIGS. 8A-8D to FIGS. 10A-10D. For the purpose of impedance matching in the coaxial aperture for band 1, the embodiment of FIG. 8B having the order of elements (from the output aperture end) as a plug, a filter, and a transformer is slightly better than the embodiment of FIG. 10B having the order of elements (from the output aperture end) as a plug, a transformer, and a filter. FIG. 8C demonstrates a return loss of −21 to −22 dB at the band edges while FIG. 10C shows approximately −20 dB.

FIGS. 11 and 12 are cross-sectional side views of dual band concentric feeds 41 and 43, respectively arranged with a lens 300. An antenna system 351 (FIG. 11) is formed by the dual band concentric feed 41 and the lens 300. An antenna system 352 (FIG. 12) is formed by the dual band concentric feed 43 and the lens 300. The inner conductive tube 125 is filled with a dielectric material 121. The dual band concentric feed 41 in FIG. 11 is arranged so that that a shared axis 400 (i.e., the Z axis of FIG. 2A) of the dual band concentric feed 41 is parallel to and overlaps a radius represented generally at R of the lens 300. Similarly, the dual band concentric feed 43 in FIG. 12 is arranged so that that the shared axis 400 of the dual band concentric feed 43 is parallel to and overlaps the radius R of the lens 300. In one implementation of this embodiment, a plurality of dual band concentric feeds 41 and/or 43 are arranged around at least a portion of the outer surface of the lens 300. In this latter embodiment, extensions of the plurality of shared axes 400 of the plurality of dual band concentric antenna feeds 41 and/or 43 intersect at the center of the lens 300.

A portion 122 of the dielectric material 121 extends beyond the aperture plane (X_{out}, Y_{out}) (FIGS. 1 and 2A) of the dual band concentric feeds 41 and 43. The portion 122 is also referred to herein as a dielectric tip 122.

FIG. 11 shows a cross-sectional side view of the dual band concentric feed 41 (FIGS. 9A-9D) with plug 169 arranged with the lens 300. The dual band concentric antenna feed 41 is designed for peak gain, crossover gain, and axial ratio for a second band. The antenna beam of FIG. 11 has a pattern angle of α.

In a switched beam antenna system, multiple feeds are available so that the feed producing the highest antenna gain in an intended direction can be selected. The pattern angle where two adjacent antenna beams intersect is a crossover angle since it is the best angular location for the beam pointing algorithm to "crossover" from one antenna beam (or feed) to the next. The crossover gain is the gain value at these crossover angles. As shown in FIGS. 13 and 14, exemplary crossover angles are $\pm\phi$. In this case, the adjacent beams (not shown) from a plurality of dual band concentric feeds arranged around at least a portion of the outer surface of the lens **300** would start with the same crossover gain. In such an embodiment, the N beam patterns, taken as a group, cover an angular range of $\pm N\phi$.

FIG. **12** shows a cross-sectional side view of the dual band concentric feed **43** (FIGS. **10**A-**10**D) with plug **170** arranged with the lens **300**. The dual band concentric antenna feed **43** is designed for peak gain, crossover gain, and axial ratio for a second band. The antenna beam of FIG. **12** also has a pattern angle of α.

FIG. **13** shows plots **310** and **311** of the second frequency band antenna gain pattern for the dual band concentric feed and lens of FIG. **11** and FIG. **12**, respectively. The solid curve of plot **311**, which is associated with FIG. **12**, has a higher crossover gain at $+\phi$ and $-\phi$ than the dashed curve of plot **310**, which is associated with FIG. **11**. The solid curve of plot **311** has a lower peak gain at pattern angle of zero degrees (0°) than the dashed curve of plot **310**.

FIG. **14** shows plots **320** and **321** of the axial ratio for the dual band concentric feeds and lens of FIG. **11** and FIG. **12**, respectively, when excited through an ideal circular polarizer. The plots **320** and **321** are for the second frequency band (e.g., at frequencies greater than f_3 as shown in FIG. **4**). The gain level of the pattern shoulders (at pattern angles $+\phi$ and $-\phi$) and the peak gain (at pattern angle 0°) are controlled by the location of the filter **150** with reference to the plug (e.g., plug **169** or **170**). Additionally, the dielectric loading provided by the plug (e.g., plug **169** or plug **170**) affects the wave propagation constant of the coaxial waveguide (e.g., the coaxial waveguide **110** in of the dual band concentric antenna **41** shown in FIG. **1**, or the coaxial waveguide **110** in of the dual band concentric antenna **43** shown in FIG. **12**) in the region occupied by the plug. Thus, controlling the length of the plug is another method for controlling the electrical location of the filter **150** within the coaxial waveguide in the dual band concentric antenna feed in the second frequency band.

In the second frequency band, the electromagnetic wave propagates through the circular waveguide **120** and radiates from the dielectric tip **122**. Some band 2 energy in the vicinity of the tip **122** enters the coaxial waveguide **110** near the end of the plug and propagates toward the filter **150** where the band 2 energy is completely reflected due to the excellent band 2 rejection properties of the filter **150** as shown in FIG. **4**. The reflected band 2 energy propagates through the coaxial waveguide **110** to the end of the feed (output aperture **180** shown in FIGS. **1** and **2**A) where it recombines with the original propagated band 2 signal, is focused by the lens **300**, and radiates into free space. The phase delay caused by the propagation and reflection of the band 2 wave in the coaxial waveguide **110** forward of the filter **150** (e.g., between the filter **150** and the output aperture **180**) is used to optimize the antenna gain pattern for band 2 frequencies.

FIG. **14** shows that the band 2 axial ratio of an antenna that is fed by a dual band concentric antenna feed **41** or **43** (FIG. **11** or **12**) coupled to the lens **300** is significantly reduced with proper selection of the filter position and plug length. FIG. **14** also shows that the axial ratio of an antenna that is fed by a dual band concentric antenna feed **41** or **43** (FIG. **11** or **12**) coupled to the lens **300** is significantly reduced with proper selection of the filter position and plug length.

EXAMPLE EMBODIMENTS

Example 1 includes a dual band concentric antenna feed comprising: an outer conductive tube having an inner surface; an inner conductive tube having an outer surface, the inner conductive tube positioned inside the outer conductive tube and coaxially aligned to a shared axis that extends a length of the outer conductive tube and the inner conductive tube, wherein a coaxial waveguide formed in a space between the inner surface of the outer conductive tube and the outer surface of the inner conductive tube supports a first frequency band, and wherein a circular waveguide formed within an inner surface of the inner conductive tube supports a second frequency band; at least one transformer in the coaxial waveguide; a filter in the coaxial waveguide, the filter being offset from the at least one transformer, wherein an impedance locus associated with the filter is high-frequency capacitive within the first frequency band and low-frequency inductive within the first frequency band; and a plug in the coaxial waveguide, the plug being offset from the at least one transformer and the filter and positioned near an aperture end of the concentric antenna feed.

Example 2 includes the dual band concentric antenna feed of Example 1, further comprising a dielectric material filling the inner conductive tube.

Example 3 includes the dual band concentric antenna feed of Example 2, wherein a portion of the dielectric material filling the inner conductive tube extends beyond the aperture plane to form a dielectric tip.

Example 4 includes the dual band concentric antenna feed of any of Examples 1-3, wherein the at least one transformer in the coaxial waveguide comprises: a first transformer in series with the plug; and a second transformer in series with the first transformer and the plug, wherein an input impedance looking into an equivalent circuit of the first transformer, the second transformer, the plug, and a shunt coaxial aperture impedance is low-frequency capacitive in the first frequency band and is high-frequency inductive in the first frequency band.

Example 5 includes the dual band concentric antenna feed of Example 4, wherein the first transformer is positioned between the plug and the second transformer, and wherein the second transformer is positioned between the filter and the first transformer.

Example 6 includes the dual band concentric antenna feed of Example 5, wherein the plug has a length of 90 electrical degrees, and wherein the shunt coaxial aperture impedance is matched across the first frequency band.

Example 7 includes the dual band concentric antenna feed of any of Examples 4-6, wherein the first transformer is formed from a dielectric ring and the second transformer is formed in the coaxial waveguide as a protrusion of the outer surface of the inner conductive tube.

Example 8 includes the dual band concentric antenna feed of any of Examples 4-7, wherein the first transformer is formed in the coaxial waveguide as a first protrusion on the outer surface of the inner conductive tube and the second transformer is formed in the coaxial waveguide as a second protrusion on the outer surface of the inner conductive tube, wherein a first gap is between the first protrusion and the inner surface of the outer conductive tube, and wherein a second gap is between the second protrusion and the inner surface of the outer conductive tube.

Example 9 includes the dual band concentric antenna feed of any of Examples 4-8, wherein the first transformer is formed from a dielectric ring and the second transformer is formed from a dielectric ring.

Example 10 includes the dual band concentric antenna feed of any of Examples 1-9, wherein the plug has a length of 90 electrical degrees, and wherein a shunt coaxial aperture impedance is matched across the first frequency band.

Example 11 includes the dual band concentric antenna feed of any of Examples 1-10, wherein the at least one transformer in the coaxial waveguide comprises: a transformer, wherein the filter is positioned between the transformer and the plug, and wherein a length of the plug is optimized to increase a crossover gain in the second frequency band and decrease an axial ratio in the second frequency band.

Example 12 includes the dual band concentric antenna feed of Example 11, wherein the plug has a length of 90 electrical degrees in the first frequency band, wherein the input return loss across the first frequency band is less than −20 dB.

Example 13 includes the dual band concentric antenna feed of any of Examples 11-12, wherein the plug has a length of 40 electrical degrees in the first frequency band.

Example 14 includes an antenna system comprising: a dual band concentric antenna feed including: an outer conductive tube having an inner surface; an inner conductive tube having an outer surface, the inner conductive tube positioned inside the outer conductive tube and coaxially aligned to a shared axis that extends a length of the outer conductive tube and the inner conductive tube, wherein a coaxial waveguide formed in a space between the inner surface of the outer conductive tube and the outer surface of the inner conductive tube supports a first frequency band, and wherein a circular waveguide formed within an inner surface of the inner conductive tube supports a second frequency band; at least one transformer in the coaxial waveguide; a filter in the coaxial waveguide, the filter being offset from the at least one transformer, wherein an impedance locus associated with the filter is high-frequency capacitive within the first frequency band and low-frequency inductive within the first frequency band; and a plug in the coaxial waveguide, the plug being offset from the at least one transformer and the filter, the plug filling a space between the outer surface of the inner conductive tube and the inner surface of the outer conductive tube at an aperture plane, the antenna system further comprising: a lens having a radius, wherein a distance between the aperture plane and the lens is selected to provide a desired antenna beam pattern, and wherein an extension of the shared axis of the dual band concentric feed is parallel to and overlaps the radius of the lens.

Example 15 includes the antenna system of Example 14, further comprising a dielectric material filling the inner conductive tube.

Example 16 includes the antenna system of any of Examples 14-15, wherein the at least one transformer in the coaxial waveguide comprises: a first transformer in series with the plug; and a second transformer in series with the first transform and the plug, wherein an input impedance looking into an equivalent circuit of the first transformer, the second transformer, the plug, and a shunt coaxial aperture impedance is low-frequency capacitive in the first frequency band and is high-frequency inductive in the first frequency band.

Example 17 includes the antenna system of Example 16, wherein the first transformer is formed from a dielectric ring and the second transformer is formed as a protrusion in the coaxial waveguide.

Example 18 includes the antenna system of any of Examples 16-17, wherein the first transformer is formed from a protrusion in the coaxial waveguide and the second transformer is formed as a protrusion in the coaxial waveguide, wherein a first gap is between the first transformer and the inner surface of the outer conductive tube, and wherein a second gap is between the second transformer and the inner surface of the outer conductive tube.

Example 19 includes the antenna system of any of Examples 14-18, wherein the at least one transformer in the coaxial waveguide comprises: a transformer, wherein the filter is positioned between the transformer and the plug, and wherein a length of the plug is optimized to increase a crossover gain in the second frequency band and decrease an axial ratio in the second frequency band.

Example 20 includes a dual band concentric antenna feed comprising: an outer conductive tube having an inner surface; an inner conductive tube having an outer surface, the inner conductive tube positioned inside the outer conductive tube and coaxially aligned to a shared axis that extends a length of the outer conductive tube and the inner conductive tube, wherein a coaxial waveguide formed in a space between the inner surface of the outer conductive tube and the outer surface of the inner conductive tube supports a first frequency band, and wherein a circular waveguide formed within an inner surface of the inner conductive tube supports a second frequency band; a first transformer in the coaxial waveguide; a second transformer in the coaxial waveguide; a filter in the coaxial waveguide, wherein an impedance locus associated with the filter is high-frequency capacitive within the first frequency band and low-frequency inductive within the first frequency band; and a plug in the coaxial waveguide, the plug filling a space between the outer surface of the inner conductive tube and the inner surface of the outer conductive tube at an aperture plane, the plug having an electrical length of 90 degrees in the first frequency band, wherein the first transformer is positioned between the plug and the second transformer, the second transformer is positioned between the first transformer and the filter, and wherein an input impedance looking into an equivalent circuit of the first transformer, the second transformer, the plug, and a shunt coaxial aperture impedance is low-frequency capacitive in the first frequency band and is high-frequency inductive in the first frequency band.

Although specific embodiments have been illustrated and described herein, it will be appreciated by those of ordinary skill in the art that any arrangement, which is calculated to achieve the same purpose, may be substituted for the specific embodiment shown. This application is intended to cover any adaptations or variations of the present invention. Therefore, it is manifestly intended that this invention be limited only by the claims and the equivalents thereof.

What is claimed is:

1. A dual band concentric antenna feed comprising:

an outer conductive tube having an inner surface;

an inner conductive tube having an outer surface, the inner conductive tube positioned inside the outer conductive tube and coaxially aligned to a shared axis that extends a length of the outer conductive tube and the inner conductive tube, wherein a coaxial waveguide formed in a space between the inner surface of the outer conductive tube and the outer surface of the inner conductive tube supports a first frequency band, and wherein a circular waveguide formed within an inner surface of the inner conductive tube supports a second frequency band;

at least one transformer in the coaxial waveguide;

a filter in the coaxial waveguide, the filter being offset from the at least one transformer, the filter designed so that, when the filter is evaluated independently over a first frequency band, with respect to an input port of the filter and with respect an output port of the filter, the filter is inductive at frequency f_1, capacitive at frequency f_2, and is well matched near frequency $(f_1+f_2)/2$; and

a dielectric plug in the coaxial waveguide, the plug being offset from the at least one transformer and the filter and positioned near an aperture end of the concentric antenna feed.

2. The dual band concentric antenna feed of claim **1**, further comprising a dielectric material filling the inner conductive tube.

3. The dual band concentric antenna feed of claim 2, wherein a portion of the dielectric material filling the inner conductive tube extends beyond the aperture plane to form a dielectric tip.

4. The dual band concentric antenna feed of claim 1, wherein the at least one transformer in the coaxial waveguide comprises:

a first transformer in series with the plug; and

a second transformer in series with the first transformer and the plug, wherein an input impedance looking into an equivalent circuit of the first transformer, the second transformer, the plug, and a shunt coaxial aperture impedance is low-frequency capacitive in the first frequency band and is high-frequency inductive in the first frequency band.

5. The dual band concentric antenna feed of claim 4, wherein the first transformer is positioned between the plug and the second transformer, and wherein the second transformer is positioned between the filter and the first transformer.

6. The dual band concentric antenna feed of claim 5, wherein the plug has a length of a quarter of a guide wavelength at $(f_1+f_2)/2$, and wherein the shunt coaxial aperture impedance is matched across the first frequency band.

7. The dual band concentric antenna feed of claim 4, wherein the first transformer is formed from a dielectric ring and the second transformer is formed in the coaxial waveguide as a protrusion of the outer surface of the inner conductive tube.

8. The dual band concentric antenna feed of claim 4, wherein the first transformer is formed in the coaxial waveguide as a first protrusion on the outer surface of the inner conductive tube and the second transformer is formed in the coaxial waveguide as a second protrusion on the outer surface of the inner conductive tube, wherein a first gap is between the first protrusion and the inner surface of the outer conductive tube, and wherein a second gap is between the second protrusion and the inner surface of the outer conductive tube.

9. The dual band concentric antenna feed of claim 4, wherein the first transformer is formed from a dielectric ring and the second transformer is formed from a dielectric ring.

10. The dual band concentric antenna feed of claim 1, wherein the plug has a length of a quarter of a guide wavelength at $(f_1+f_2)/2$, and wherein a shunt coaxial aperture impedance is matched across the first frequency band.

11. The dual band concentric antenna feed of claim 1, wherein the at least one transformer in the coaxial waveguide comprises:

a transformer, wherein the filter is positioned between the transformer and the plug, and wherein a length of the plug is optimized to increase a crossover gain in the second frequency band and decrease an axial ratio in the second frequency band.

12. The dual band concentric antenna feed of claim 11, wherein the plug has a length of a quarter of a guide wavelength at $(f_1+f_2)/2$ in the first frequency band, wherein the input return loss across the first frequency band is less than −20 dB.

13. The dual band concentric antenna feed of claim 11, wherein the plug has a length of 40 electrical degrees in the first frequency band.

14. An antenna system comprising:

at least one dual band concentric antenna feed including:

an outer conductive tube having an inner surface;

an inner conductive tube having an outer surface, the inner conductive tube positioned inside the outer conductive tube and coaxially aligned to a shared axis that extends a length of the outer conductive tube and the inner conductive tube, wherein a coaxial waveguide formed in a space between the inner surface of the outer conductive tube and the outer surface of the inner conductive tube supports a first frequency band, and wherein a circular waveguide formed within an inner surface of the inner conductive tube supports a second frequency band;

at least one transformer in the coaxial waveguide;

a filter in the coaxial waveguide, the filter being offset from the at least one transformer, wherein an impedance locus associated with the filter is high-frequency capacitive within the first frequency band and low-frequency inductive within the first frequency band; and

a dielectric plug in the coaxial waveguide, the plug being offset from the at least one transformer and the filter, the plug filling a space between the outer surface of the inner conductive tube and the inner surface of the outer conductive tube at an aperture plane, the antenna system further comprising:

a lens having a radius, wherein at least one distance between the respective at least one aperture plane of the at least one dual band concentric antenna feed and the lens is selected to provide a desired antenna beam pattern, and wherein an extension of the shared axis of the dual band concentric feed is parallel to and overlaps the radius of the lens.

15. The antenna system of claim 14, further comprising a dielectric material filling the inner conductive tube.

16. The antenna system of claim 14, wherein the at least one transformer in the coaxial waveguide comprises:

a first transformer in series with the plug; and

a second transformer in series with the first transform and the plug, wherein an input impedance looking into an equivalent circuit of the first transformer, the second transformer, the plug, and a shunt coaxial aperture impedance is low-frequency capacitive in the first frequency band and is high-frequency inductive in the first frequency band.

17. The antenna system of claim 16, wherein the first transformer is formed from a dielectric ring and the second transformer is formed as a protrusion in the coaxial waveguide.

18. The antenna system of claim 16, wherein the first transformer is formed from a protrusion in the coaxial waveguide and the second transformer is formed as a protrusion in the coaxial waveguide, wherein a first gap is between the first transformer and the inner surface of the outer conductive tube, and wherein a second gap is between the second transformer and the inner surface of the outer conductive tube.

19. The antenna system of claim 14, wherein the at least one transformer in the coaxial waveguide comprises:

a transformer, wherein the filter is positioned between the transformer and the plug, and wherein a length of the plug is optimized to increase a crossover gain in the second frequency band and decrease an axial ratio in the second frequency band.

20. A dual band concentric antenna feed comprising:

an outer conductive tube having an inner surface;

an inner conductive tube having an outer surface, the inner conductive tube positioned inside the outer conductive tube and coaxially aligned to a shared axis that extends a length of the outer conductive tube and the inner conductive tube, wherein a coaxial waveguide formed in a space between the inner surface of the outer conductive tube and the outer surface of the inner conductive tube supports a first frequency band, and wherein a circular waveguide formed within an inner surface of the inner conductive tube supports a second frequency band;

a first transformer in the coaxial waveguide;

a second transformer in the coaxial waveguide;

a filter in the coaxial waveguide, the filter designed so that, when the filter is evaluated independently over a first frequency band, with respect to an input port of the filter and with respect an output port of the filter, the filter is inductive at frequency f_1, capacitive at frequency f_2, and is well matched near frequency $(f_1+f_2)/2$; and

a dielectric plug in the coaxial waveguide, the plug filling a space between the outer surface of the inner conductive tube and the inner surface of the outer conductive tube at an aperture plane, the plug having a length of a quarter of a guide wavelength at $(f_1+f_2)/2$ in the first frequency band, wherein the first transformer is positioned between the plug and the second transformer, the second transformer is positioned between the first transformer and the filter, and wherein an input impedance looking into an equivalent circuit of the first transformer, the second transformer, the plug, and a shunt coaxial aperture impedance is low-frequency capacitive in the first frequency band and is high-frequency inductive in the first frequency band.

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